



# Observed F-16 and F-17 Anomalies Detailed Analysis of the Root Causes, and the Path Forward

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- Description of the Calibration Anomalies
- Post-Launch Mitigation Strategies
- Analysis and Verification of Root Causes
- Path Forward for F-18 through F-20 SSMIS





#### F-16 Calibration Issues

### **Reflector Emission**

- Reflector Rim Temperature Cycle Dominated by Earth and Spacecraft Shadowing
- OB-BK Patterns Showed Frequency Dependent Reflector Emissivity,  $\epsilon_{\text{Rflct}}$ 
  - 1.5–2K OB-BK Jump at 50-60 GHz
  - 5-7K OB-BK Jump at 183 GHz

### Warm Load Intrusions

- Direct and Reflected Solar Intrusions onto Warm Load Tines
- 1-1.5K Depression in TBs
- Field-of-View Obstructions
- Moon Intrusion into Cold Sky Reflector
- Random Noise Spikes

### F-17 Calibration Issues

#### **Reflector Emission**

- Reflector Rim Thermistor moved to rear of graphite epoxy reflector shell
- Reflector Temperature Cycle Dominated by Solar Panel Shadowing for Most of Year, Some Earth and Spacecraft Shadowing
- Frequency Dependent Reflector Emissivity,  $\epsilon_{Rflct}$ 
  - 1.5–2K OB-BK Jump at 50-60 GHz
  - 5-7K OB-BK Jump at 183 GHz

### Warm Load Intrusions

- Fence Successful in Mitigating Direct Solar Intrusions
- Reflected Solar Intrusions onto Warm Load Tines limited to High Solar Elevation angles
- Residual Doppler Signature
- Additional Noise due to Flight S/W Mods, Fewer Calibration Samples
- Field-of-View Obstructions
- Moon Intrusion into Cold Sky Reflector
- Random Noise Spikes





### SSMIS Calibration Anomaly Detection

 Using OB-BK computed using ECWMF analyses and RTTOV-8 in combination with the DGS software package developed by Mike Werner (Aerospace), the SSMIS Cal/Val team was able to pinpoint the physical mechanisms causing the Calibration Anomalies

















## Summary of the SSMIS Calibration Anomalies F-16 versus F-17 Scan-to-Scan Noise Levels









### NRL/Met Office SSMIS Unified Pre-Processor (UPP) Overview

Unified Pre-Processor designed to mitigate the calibration anomalies uncovered during the SSMIS Cal/Val process and produce corrected SSMIS TDR files suitable for radiance assimilation at both global and regional scales.

- UPP V1 included
  - Reflector Emission Corrections
  - Warm Load Solar Intrusion detection and flagging (Gain Anomalies)
  - Spatial Averaging to reduce NE $\Delta$ T to the 0.1 K level
- UPP V2 includes
  - Uses Operational NGES Fourier Filtered Gain Files to Correct Gain Anomalies
  - Produces ASCII and BUFR TDR output files at reduced resolution
  - Performs Scan Non-uniformity corrections
- UPP V3 Plans
  - Perform Anomaly corrections and produce TDR file at native resolution
  - Allow end-users to define amount of spatial averaging
  - Additional F-17 Calibration Averaging to lower scene noise







PRECISE EFFECTIVE CONDUCTIVITY MEASUREMENTS OF REFLECTOR SURFACES USING CYLINDRICAL TE01 MODE RESONANT CAVITIES

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For Large Effective Conductivities, the approximate  $\nu$  and h polarized emissivities are:

$$\varepsilon_v \cong \sqrt{\frac{16\pi \upsilon \varepsilon_0}{\sigma}} \sec \theta_i$$

- U : Frequency [Hz]
- $\mathcal{E}_0 \quad \begin{array}{c} : \text{ Free-space permittivity} \\ \text{ [F/m]} \end{array}$
- $\theta_i$  : Surface Incidence angle

Ideally, we want an  $\epsilon_{Rflct}$  approaching that of Pure Al

$$\varepsilon_h \cong \varepsilon_v \cos^2 \theta_i$$

Effective Conductivity,  $\sigma$  [MS/m]

Example:

183 GHz Pure Al at 300 K  $\Theta_i = 18^\circ$   $\sigma = 36.59$  MS/m  $\mathcal{E}_v = 0.00157$ 

 $\varepsilon_{h} = 0.00142$ 





Resonant Cavity Measurements have been conducted at 7 and 32 GHz, for Reflector coupons from the following sensors

Mission	Test Coupon	Effective Conductivity [MS/m]	Emissivity at 32 GHz	Emissivity at 183 GHz*
JIMO+(Jupiter Icy Moons)	Coupon 1	32±1	0.0006	0.0014
CloudSat+	Flight Unit	2.11±0.03	0.0023	0.0056
JMR	Spare–Post rework	15.1±0.5	0.0008	0.0021
(Jason Microwave Radiometer)	Spare–Post rework	14.6±0.5	0.0009	0.0021
	Spare–Post rework	0.353±0.004	0.0057	0.0137
	Flight Unit	9±2	0.0013	0.0027
MLS	Flight Unit	4.3±0.1	0.0016	0.0039
AMR	Original Coupons	0.2	0.0076	0.0183
Advanced Microwave	Prior to rework	1.4	0.0029	0.0069
Radiometer		3.4	0.0185	0.0044
OSTM Launch		9.1	0.0011	0.0027
~ June 2008		16.5	0.0008	0.0020
		31.	0.0006	0.0015

<sup>+</sup> Active Radars

#### \* Computed form the 32 GHz measurement





## VDA Applied to Aggressively Roughened Surface

VDA\* Layer

Carbon Fibers of the Unidirectional Cross-Layered Tape (P75S/ERL1962) forming the Epoxy Shell



32 GHz  $\sigma_{\rm E}$  = 3.4 MS/m 55 GHz ε = 0.0027

**\*VDA: Vapor Deposited Aluminum** 





## VDA Applied to Moderately Roughened Surface

VDA Layer-

Carbon Fibers of the Unidirectional Cross-Layered Tape (P75S/ERL1962) forming the Epoxy Shell



32 GHz  $\sigma_{\rm E}$  = 9.1 MS/m 55 GHz ε = 0.0016





## VDA Applied to Smooth Surface













• NWP and visualisation tools key to understanding and mitigating instrument calibration anomalies

• Pre-processing (UPP) required to meet stringent requirements of NWP radiance assimilation users for temperature sounding

• New measurement techniques have been developed for pre-launch characterisation of reflectors, and should reduce risk for future radiometers

• Original F-18 Reflector has been replaced with Spare Reflector (15-18 MS/m)

• DMSP SPO plans to either Strip and Recoat the F-19 and F-20 Reflectors or manufacture new reflectors





## **Backup Slides**



## SSMIS Warm Load Calibration Samples Early Orbit Mode Data





- Saw-tooth pattern is the result of the A/B Integrator
- Original Flight S/W averaged 4 warm load samples
- F-17 Flight S/W changes now use only 2 warm load samples
- Additional warm load samples (8-12) would lower noise
- Lower noise is crucial to NWP radiance assimilation

EO-2 Mode Imagery, courtesy of Dave Kunkee, Aerospace



**AMSU OB-BK Biases** 



### Un-corrected OB-BK



AMSU also contains biases, which must be removed prior to assimilation. AMSU OB-BK biases are dominated by scan angle effects and air mass biases in the RTM. Biases are also sensor specific.





Both F-16 and F-17 SSMIS Exhibit Calibration Anomalies which are unique to the each sensor and orbit geometry

Over 40% of F-16 SSMIS Data are Affected by the Calibration Anomalies

- Reflector Emission Biases
- Warm Load Intrusions

All of F-17 SSMIS Data are Affected by the Calibration Anomalies/Issues

- Reflector Emission Biases
- Increased Noise due to Calibration Flight S/W Mods
- Warm Load Intrusions Limited to High Solar Elevation periods
- Channel 4 Cold Cal Count Problem (Synthetic Cold Cal a possibility)

Preprocessing of SSMIS Radiance Data for Operational NWP DAS for the Temperature and Humidity sensitive channels is a Requirement





- F-16 UPP V2 is Operational at FNMOC and is being Distributed to NESDIS
- UPP V2 includes the required BUFR Format modification Option
- NRL has Transitioned F-16 SSMIS UPP to FNMOC for Radiance Assimilation
- F-17 UPP Modifications Underway
- AFWA currently conducting WRF Radiance Assimilation Trials using the UPP V2 data in for the Southeast Asia window corresponding to the FNMOC/AFWA JEFS/JME demonstration project this past Summer
- EMC conducting GFS Radiance Assimilation Trials using the UPP V2
- Met Office is Operational with SSMIS Met Office PP, and plans to wait for operational distribution of UPP by FNMOC
- EMC, ECMWF, MeteoFrance, and MSC plan on using data from the SSMIS UPP V2 as soon as its available





SSMIS Unified Preprocessor Developed to Meet NWP DA Needs

The UPP Produces SSMIS data that Meet the Stringent NWP Radiance Assimilation Accuracy Requirements for Temperature Sounding Channels

Plans are to allow for user specified Averaging to meet specific application requirements. i.e. Mesoscale NWP

SSMIS UAS Radiance Assimilation will also Require Pre-Processed SSMIS TDR data with the required Geomagnetic Parameters

F-17 SSMIS Data Present an New Challenge for the Radiance Assimilation Community to Produce TDR Data meeting the NWP DA Requirements





SSMIS Reflector Emission Bias,  $\Delta T_{Emis}$   $T_{Obsvd} = (1 - \varepsilon_{Rflct})T_{Scene} + \varepsilon_{Rflct}T_{Rflct}$   $T_{Scene} = T_{Obsvd} - \varepsilon_{Rflct}(T_{Rflct} - T_{Scene})$  $\Delta T_{Emis} = T_{Obsvd} - T_{Scene} = \varepsilon_{Rflct}(T_{Rflct} - T_{Scene})$ 

- Caused by a frequency dependent reflector emissivity,  $\epsilon_{Rflct}$  that is much larger than expected based upon pre-flight assumptions regarding a graphite epoxy reflector shell coated with a multiple layers of VDA Al and SiO<sub>x</sub>.
- Post-Launch analysis of OB-BK signatures indicate the peak Emission Bias is of the order 1.5-2 K for the 50-60 GHz channels and 5-7 K for the 183 GHz channels
- Provided the reflector temperature  $T_{Rflct}$  and  $\epsilon_{Rflct}$  are known, a Reflector emission correction can be applied
- Given a Solar Absorptivity/IR emissivity ( $\alpha/\epsilon$ ) ratio = 0.8 for SiO<sub>x</sub>, Maximum  $T_{Rflct}$  should be ~O(300 K)







$$\Delta T_{Emis} = \varepsilon_{Rflct} \left( T_{Rflct} - T_{Scene} \right) = \varepsilon_{Rflct} \left( T_{Rflct} - 210 \right)$$









$$\Delta T_{Emis} = \varepsilon_{Rflct} \left( T_{Rflct} - T_{Scene} \right) = \varepsilon_{Rflct} \left( T_{Rflct} - 240 \right)$$







## AMR and SSMIS Conductivity Measurements

• Measured Effective Conductivities were anomalously low compared to Pure AI (37.7 MS/m) for additional coupons measured from previous AMR developments and other instruments

• Parallel materials investigation indicated a correlation between poor RF performance and level of surface roughening applied to composite layer

• AMR investigation coupled with SSMIS investigation indicates that a reliable coating process needs to be defined and verified

• Current VDA surface coating process produces RF surfaces guaranteed to perform somewhere between that of pure aluminum and bare graphite epoxy composite

• Clearly, a more precise and repeatable reflector coating process is required for space based precision microwave radiometers





Resonant Cavity Measurements have been conducted at 32 GHz, for SSMIS and Re-Worked AMR Reflector coupons

Mission	Test Coupon	Effective Conductivity [MS/m]	Emissivity at 32 GHz	Emissivity at 183 GHz+
Re-Worked AMR Coupons	4 Coupons with Minor Surface Abrasion	18 – 20	0.00076- 0.0008	0.0019
	No Surface Abrasion	19-20	0.00078-0.0008	0.0018-0.0019
SSMIS	Mass Model (Bare Graphite Epoxy)	0.0394-0.044	0.016-0.017	0.039-0.041
	SN03	0.54 – 1.119	0.0032-0.0046	0.0077-0.011
	SN04	0.144 – 0.231	0.0071-0.009	0.017-0.022
	Spare Reflector*	15.1-17.4	0.0008-0.0009	0.0019-0.0021
	CSR	2.7-3.4	0.0018-0.0021	0.0044-0.005

\* SSMIS Spare Reflector manufactured by Composite Optics, but with Grit Blast vice Cabosil Primer to enhance VDA adhesion

+ The Emissivity at 183 GHz does not include surface roughness effects, and should be considered a lower bound on the 183 GHz emissivity International TOVS Study Conference, 16<sup>th</sup>, ITSC-16, Angra dos Reis, Brazil, 7-13 May 2008. Madison, WI, University of Wisconsin-Madison, Space Science and Engineering Center, Cooperative Institute for Meteorological Satellite Studies, 2008.