

RAINFALL ESTIMATION FROM GEOSTATIONARY
SATELLITE IMAGES OVER THE GATE AREA

A REPORT

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John Stout
David W. Martin

Space Science and Engineering Center
University of Wisconsin
1225 West Dayton Street
Madison, Wisconsin 53706

Dhirendra N. Sikdar

Geological Sciences Department
University of Wisconsin
3409 North Downer Street
Milwaukee, Wisconsin 53201

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I. Introduction

Rainfall is important to the 1974 (GATE) Atlantic Tropical Experiment because it is a large term in budgets of moisture in disturbed conditions, and because it represents the amount and distribution of heat released through condensation (1, 2, 3). Anticipating the difficulty of adequately measuring rainfall with rain gages, in the design of GATE there was an emphasis on remote systems (1, 2).

The most successful of these remote systems has been radar. Four C-band radars provided excellent rainfall information over the inner (B-scale) ship hexagon and the area adjacent the B-array (4). But these radars could not provide rainfall information to the outer (A/B-scale) ship hexagon, nor, of course, to the larger area of the A-scale ships. Coverage on the larger A/B and A scales was left to satellites--the microwave sensor on Nimbus 5, and the visible-infrared sensors on the first Synchronous Meteorological Satellite. Nimbus 5 sampled at a fairly coarse time and space resolution, days and tens of kilometers (5). The sampling of SMS-1, on the other hand, was more like that of the radars, and therefore offered a way to extend the convective scale radar measurements of rainfall to the A/B ship array, and beyond, to the whole A-scale tropical north Atlantic.

Estimates of rainfall on the A-scale are being made by the Cumulus Group of NOAA's National Hurricane and Experimental Meteorology Laboratory (6). The concern of this report is estimates of hourly rainfall for individual convective rain systems occurring within and around the A/B array.

The program to provide satellite estimates of GATE area rainfall has existed at SSEC since 1972. It's objectives are threefold: to develop a

technique for estimating GATE area rainfall using images of the SMS geostationary satellite; to test that technique; and to provide estimates of rainfall for use by the GATE research community. Collaboration has been maintained with the Cumulus Group, NHEML, especially in the development stages of the program.

The work done at Wisconsin is summarized in a series of annual reports and a conference postprint paper; these are listed with other references at the end of this report (7, 8, 9, 10, 11). A joint NHEML-SSEC paper (6) describing the general approach and test results has been submitted to Monthly Weather Review. The present report describes the method in the configuration it has assumed at Wisconsin. Because this is a final report, we have tried to provide an overview, including the basis of the method, its development, and tests of accuracy. In this report we also present, as maps and tables, satellite estimates of rainfall for several days from the third phase of GATE.

II. Physical Basis

Several years ago Sikdar (12) found expansion of the cirrus canopy atop deep convective clouds to be a measure of volumetric rainfall. More recently Griffith and Woodley (13) and Reynolds and Vonder Haar (14) confirmed a positive relationship between convective cloud thickness and cloud brightness. To the extent that cloud thickness is proportional to rainfall, this latter finding suggests rainfall also is related to brightness. Indeed, this has been found to be true, for example, when radar echoes are compared with satellite clouds (15, 16, 17, 18), but the association with rainfall is best for growing clouds, that is, deep convective clouds in early and mature stages of development (7, 8, 19).

The physical basis for the relationship between convective cloud brightness and rainfall remains obscure. Some direct measurements of cloud albedo (20, 21) indicate that saturation is reached with optical thicknesses which are small compared with the optical thickness of a deep convective cloud. McKee and Cox (22) argue that the satellite observed increase in brightness of deeper clouds is a consequence of a smaller loss of light through the sides owing to the larger diameter of deeper clouds. Quite recently Mosher (communicated) has begun a series of tests of the brightness of theoretical finite clouds of various shapes and configurations. Mosher finds that the pattern of brightness observed from satellites for cumulonimbi can be explained using different droplet concentrations for the cloud core and the anvil. This work is continuing.

The early studies relating bright clouds to echoes encouraged a straightforward approach to the problem of inferring rainfall from satellite images: simple correlation of cloud area A against volumetric rain rate R. To account for changes in rain production through the life history of convective clouds, the relationship was made time dependent. It can be expressed as

$$R(t) = k(t) A(t), \quad (1)$$

where t refers to stage of development. Because the coefficient k is a complicated function, its value ordinarily is determined graphically.

The lag observed between maximum rain rate and maximum cloud area suggested an alternative formulation involving the sum of two terms, cloud

area and the time rate of change of cloud area:¹

$$R(t) = a_0 A(t) + a_1 \frac{\Delta A}{\Delta t} \quad (2)$$

Both coefficients are constant. It is this formulation which is developed, tested, and used in our estimates of rainfall for GATE.

III. Calibration

The first step in establishing a relationship between cloud area and rainfall is to define the clouds. Cloud area (in visible wavelength images) and associated volumetric rainfall rate then are measured for individual cloud/echo systems as they evolve. Normalizing by maximum cloud area, these measurements may be combined in a graph of volumetric rainfall rate as a function of cloud area (6), or, as in the present instance, they may be combined in a least squares estimate of the coefficients a_0 and a_1 from Eqn. 2. These procedures are repeated for clouds in infrared images.

A. Defining a cloud

Selecting a threshold brightness for defining a cloud in a visible image is based on empirical relationships between maximum observed cloud brightness and probability of precipitation (6, 7, 19). The level selected for present purposes is 172 digital counts (d.c.), which is equivalent to an albedo of .47 with the sun overhead (23). This level corresponds quite

¹We are indebted to Professors H. Lettau and E. Wahl for suggesting this formulation.

closely to the level of maximum correlation between visible cloud area and volumetric rainfall rate (Fig. 1).

The level selected for infrared is 160 dc. This corresponds to an equivalent blackbody temperature of -26C. Again, the threshold level is close to the level of highest correlation between cloud area and volumetric rainfall rate (Fig. 2).

B. Measuring cloud area and rainfall

Cloud area and volumetric rainfall rate are measured with the University of Wisconsin's Man-Computer Interactive Data Access System, McIDAS (24). Satellite infrared or visible images are displayed in sequence opposite a matching radar sequence. Visible satellite images are normalized for changing sun-satellite-cloud geometry using the scheme of Mosher (9). Radar images are remapped to the scale and projection of the satellite images. A cloud is identified, and its area is measured.² When all deep convective cloud areas have been measured, the areas of the echoes associated with each cloud are measured, at intervals of 3 dbz. These measurements are used with the GATE reflectivity-rainfall relation suggested by Austin and others (25, 26), $Z = 230R^{1.25}$, to calculate volumetric rainfall rate.

The data used in calculating a_0 and a_1 are SMS-1 GATE satellite images and Oceanographer 5.3 cm PPI scans from Phase III. During Phase III the Oceanographer was stationed at 7° 45' N, 22° 12' W. The Oceanographer radar data were corrected for atmosphere attenuation, energy loss to the sea, and

²An operator uses a cursor (an electronic crosshair moved by a joystick) to draw an outline around a cloud. Then the computer calculates the area within the outline which is above the threshold brightness.

"instrument bias" (26, 27) (Appendix A). Only clouds with echoes less than 200 km from the ship were used. Data during times of heavy rain on the radome were interpolated. Measurements were made on full resolution (4 x 8 km infrared, 1 km visible, 4 km radar) digital data, for 2 days, 4 and 6 September. Twenty-three clouds were followed in visible images, giving a total of 219 paired measurements of cloud area and associated rainfall. Thirty-four clouds were followed in infrared, giving a total of 326 paired measurements of cloud area and associated rainfall.

Measurements also were made over south Florida using 1972 and 1973 image sequences from the Applications Technology Satellite (ATS-1) (7, 8), and 1974 image sequences from SMS-1 (9). Rainfall was obtained from the National Hurricane Center Miami WSR-57 10-cm radar. The ATS-1 data proved to be of poorer resolution than those from SMS-1. The relation between ATS and SMS visible brightness levels was ambiguous, and ATS rainfalls were higher than SMS Florida rainfalls. On the other hand, the SMS Florida rainfalls were lower than GATE rainfalls, owing, perhaps, to an uncertainty in the calibration of the Miami radar in 1974 (Griffith, communicated). For these reasons, we have used only GATE measurements in the determination of the coefficients a_0 and a_1 .

C. Cloud area--rainfall relations

The relationships produced from the GATE calibration measurements are

$$R = 0.52A_{vi} + 2600 \Delta A_{vi}/\Delta t \quad (3)$$

and $R = 0.54A_{ir} + 2800 \Delta A_{ir}/\Delta t \quad (4)^3$

Statistical properties of the calibration sample are given in Table 1. Note

³The coefficients in Eqn (4) differ slightly from those given in the post-print paper (11) owing to small changes made in a final editing of the data. R is in $m^3 s^{-1}$, A in km^2 , and $\Delta A/\Delta t$ in $km^2 s^{-1}$.

that although the visible and infrared coefficients are almost equal, the infrared clouds and rainfall are half again or more larger. This is consistent with the finer resolution of the visible imagery allowing better discrimination of clouds. Also noteworthy is the dominance of the area term ($a_0 \bar{A}$) over the area change term ($a_1 \overline{\Delta A/\Delta t}$). This difference is especially marked for visible clouds, implying that an instantaneous measurement of cloud area will give a better measure of rainfall rate in visible than in infrared. In addition visible measurements have a smaller variability than infrared, as measured by the ratio of root mean square rainfall rate to average rainfall rate. Thus full resolution visible image sequences are preferred for estimating rainfall; however, the problems of daytime only coverage and changing illumination usually tip the balance in favor of infrared sequences.

Table 1

Mean and root mean square values for the data sample used to calculate the visible and infrared coefficients a_0 and a_1 . RMS is for the difference between actual and estimated rain for one cloud for one half hour.

	infrared	visible	units
a_0	5.4×10^{-7}	5.2×10^{-7}	ms^{-1}
a_1	2.8×10^{-3}	2.6×10^{-3}	m
$a_0 \bar{A}$	3.3×10^3	2.3×10^3	$\text{m}^3 \text{s}^{-1}$
$a_1 \overline{\Delta A/\Delta t}$	1.0×10^3	4.2×10^2	$\text{m}^3 \text{s}^{-1}$
\bar{R}	4.7×10^3	2.9×10^3	$\text{m}^3 \text{s}^{-1}$
RMS	3.6×10^3	1.8×10^3	$\text{m}^3 \text{s}^{-1}$
RMS / \bar{R}	.76	.62	

IV. Accuracy

A. Limitations

The accuracy of this technique is limited in several respects. Most fundamentally, it proposes to estimate rainfall, the product of a very complex process, with two predictors, convective cloud area and area change. Because we cannot directly account for each of the many conditions and processes that influence rainfall, we must assume that they are reflected in area and area change, the variables which can be measured. The contribution of this assumption to total error is difficult to gage; however, this error clearly is minimized if estimates are made only for the area, season, and general synoptic conditions of the calibration data.

Inaccuracies in ground truth may contribute significantly to total error. Phase averages of the digital radar data used as ground truth for the satellite technique are believed, on the basis of radar intercomparisons and comparisons of radar rainfall with ship gage measurements, to be accurate to within 25% (28). If this error were random and normally distributed the radar measurement of rainfall for an average satellite cloud of $5,000 \text{ km}^2$ would be within 50% of the true value over the 5h life of the cloud. However, some of the 25% total error in phase mean radar rainfall is likely to be due to biases remaining despite all efforts to remove them. The 50% figure therefore is an outside estimate of probable error in the ground truth measurement of total cloud rainfall. The accuracy for any given area and period will depend on the number of cloud estimates included.

Cunning and Sax (29) offer a Z-R relation different from that used to calculate rainfall in the present study. Their exponent, 1.52, gives a rainfall rate 25% smaller at a reflectivity of 40 dbz (29), with larger

differences at higher reflectivities. However, the smaller rainfall rates at high reflectivities tend to be compensated by larger rainfall rates at low reflectivities. The difference in rainfall rate averaged over the calibration sample is likely to be small.

A third contribution to error comes in the measurement of cloud area. Over the period of GATE there was a gradual change in the sensitivity of the infrared scanner. Measurements by Lienisch, reported by Smith and Vonder Haar (30), show that over Phase III (the period of immediate interest), the drift of the infrared sensor at the cloud threshold of 160 dc was about 1.4 C. A drift of this amount produces an error of \pm 5% in the measurement of cloud area. Considering other sources, this is too small a contribution to total error to warrant correction (however, departures from the digital count to temperature relation implicit in Eqn. 4 were considerably larger earlier in GATE). A diurnal excursion of sensor sensitivity appeared with the onset of satellite eclipse on 24 August (31, 32, 33). The effect of the increased sensitivity was to decrease the blackbody temperature corresponding to 160 dc by up to 2.5 C, and thus to increase the area of a threshold cloud measurement. This error is largest just after ellipse, about 4 to 6 GMT. Typical errors in area measurement at the peak of the excursion are \pm 10%, thus, though it may be important for individual rain estimates made just after eclipse, this is a minor contributor to total error. Smith (33) has noted that the rather slow (55 μ s) response time of the infrared sensor produces a smearing as the sensor scans from warm (ocean) to cold (cirrus). This slow response and the fairly coarse resolution of the infrared scanner will combine to underestimate the areas of deep convective clouds. The effect on estimates of

rainfall can be significant for small clouds.

Scale imposes a fourth limitation on satellite estimates of rainfall. Comparisons of satellite and echo fields (e.g. 15, 16, 19) show that at the thresholds used here clouds typically are 5 or more times larger than associated echoes. This is a consequence of looking down on the clouds: the anvil registers more clearly than the cloud towers, where precipitation is concentrated (the effect is stronger in infrared than in visible images, because of the greater opacity of cloud at longer wavelengths). There are several plausible schemes for allocating rainfall. In all, however, the compromise between accuracy in location of the maximum and accuracy in extent of the rainfall tends to spread the rainfall beyond its actual limits for small clouds, but over concentrates it for large clouds.

Presently, rainfall is assigned to the location of the brightest picture element within the cloud outline. Where the gradient of brightness across the cloud is flat, or where noise is present within the digital data, this point may be distant from the actual location of the highest rainfall. Experience indicates that the separation rarely exceeds a distance equal to the equivalent radius of the cloud.

Finally, there has been concern that rainfall not originating in deep convective clouds might contribute substantially to total GATE rainfall. The satellite cloud code developed to estimate this "background" rainfall is described in Appendix B. Of some 275 one hour gage and radar observations under non-deep convective clouds, six showed measurable rain. The average rain rate for the sample was $0.01 \text{ mm} \cdot \text{hr}^{-1}$. Therefore, while background rainfall may contribute substantially to total rainfall in local areas of scattered weak convection, it is of no importance to estimates of rainfall

which include numbers of deep cumulonimbus clouds, and has not been included in estimates in this report.

B. Test results

Half hourly rainfall estimates from infrared images were made for two days, 4 and 5 September, when several intense convective disturbances occurred within the A/B-array (Fig. 3a, b). Hourly rainfall rate was calculated from the satellite estimates for the "master array", a disc 204 km in radius centered at 8°30'N, 23°30'W (the center of the B-array). These are compared as time series plots and as a scatter diagram with one hourly composite digital radar measurements of hourly rainfall rate supplied by Hudlow. About one sixth of the test sample (Oceanographer radar on 4 September) was part of the calibration sample. These data could be ignored, and the conclusions would be the same.

There is a tendency for satellite rainfall to exceed radar rainfall as rainfall peaked late on 4 September (Fig. 4). Five points on the satellite plot for 5 September are anomalously low. This is a consequence of the way satellite rainfall is allocated. In these cases the brightness peaks of two large clouds (one at 5 to 6 GMT, another at 15 GMT) fell just outside the master array, although the cloud itself straddled the boundary. The solid line ignores rainfall from this cloud. The dotted line assumes half to one third of the cloud rainfall fell within the master array. The satellite and radar rainfall plots then track very well.

Another way to view these results is as a scatter diagram of radar and satellite rainfall (Fig. 5). The five underestimates on 5 September are present as outliers to the general pattern, a band of points along the line of slope one. With all points included the regression of satellite on

radar rainfall is

$$R_s = 0.12 + 0.84 R_v$$

and the correlation is 0.68. If the five outliers from 5 September are excluded, the regression becomes

$$R_s = 0.12 + 0.89 R_v$$

and the correlation is 0.88.

A second comparison of satellite with radar rainfall was made for ten hours on 9 September. The master array was covered with cloud (Fig. 6). Initially this was middle and low cloud, with a few weak cells of convection. Small cumulonimbi increased in number through the period. Only the larger cells were measured for satellite rainfall (these cells were dwarfed by the very large rain systems lying to the north and north-east). Therefore, in spite of a six-fold increase in average rainfall rate, satellite rainfall is consistently below radar rainfall (Fig. 7). The difference, 0.1 to $0.2 \text{ mm} \cdot \text{h}^{-1}$, is believed to be largely due to the contribution of small convective clouds, rather than to a bias in the estimates of rain from the clouds that were measured. Outlining those unmeasured small clouds which did reach the 160 dc threshold would have reduced the error in the satellite estimate. However, a fraction of the actual rainfall would not have been accounted for, except by invoking background rainfall.

We conclude from these tests that for time intervals down to one hour and for scales as small as 100 km there is substantial skill in the satellite estimates of rainfall. To the extent that errors are random, accuracies can only increase with larger time periods and larger areas.

V. Product

Rain estimates have been made for several cases under investigation by the GATE community. Times and areas covered are given in Table 3. Deep convective clouds were identified and measured on infrared satellite images. A photograph of each on image from each case is shown in Fig. 3. Area measurements were converted to rain estimates with equation (4). If the estimate for a cloud at a given time was negative, it was set to zero. The estimates are displayed in two forms: a listing organized by time of location, volumetric rain rate, and cloud area of each cloud (Appendix C), and contour analyses for three hour synoptic times (Appendix D). In the analysis, estimates were assigned to the nearest gridpoint in a half degree array. The average rain rate was calculated for each gridpoint, and the whole array was contoured.⁴

Table 3
Rain estimation coverage

State	Period	Area			Time resolution
		End	West longitude	North latitude	
0330Z, 4 Sept	0200Z, 5 Sept	12-32	1-16	30 min.	
0400Z, 5 Sept	2330Z, 5 Sept	13-33	1-16	30 min.	
0430Z, 9 Sept	1630Z, 9 Sept	14-34	5-20	30 min.	
0800Z, 18 Sept	1800Z, 18 Sept	19-24	7-12	15 min.	

VI. Summary and Conclusions

Although radars provided accurate rainfall information of high time and space resolution for GATE, coverage was limited to the immediate B-array.

⁴A linear interpolation along the legs connecting the gridpoints is made to find the contour crossings. Then the series of line segments connecting these crossings is smoothed by a running average of .15 inches, which corresponds to .3 degrees on 4, 5, 9 Sept. and .15 degrees on 18 Sept.

The gages of the A/B ships are totally inadequate to the task of providing information on rain amounts and distribution between the B and A/B arrays. Only one system, the visible and infrared radiometer on board the SMS-1 satellite, provided data on the time and space scales needed to follow convective rain systems beyond the range of the radars.

It is to provide this information that the present technique was developed. Volumetric rainfall rate for a distinct convective rain system is estimated from the sum of two terms, cloud area, and area change. These are measured in a sequence of satellite images. The scale of the estimate is the scale of definable deep convective cloud systems. This is an average of 4500 km^2 for clouds in full resolution visible images, and 6000 km^2 for clouds in full resolution infrared images.

Maps and tables of satellite rainfall are presented for 4 days of special interest from Phase III of GATE. Three of these (4, 5, and 9 September) use half hour pictures and cover areas 15° in latitude by 20° in longitude. The fourth (18 September) uses quarter hour pictures and covers an area 5° by 5° .

Two tests of accuracy, using radar as ground truth, show little evidence of bias in estimates for situations of well organized deep convection. For a one hour period (two images) over an area 400 km in diameter ($1.3 \times 10^5 \text{ km}^2$) the satellite estimate of moderate to heavy convective rainfall might be expected to differ from the radar measurement by a factor of 0.6 to 1.8. since random error is an inverse function of sample size, accuracy should improve for longer periods and larger areas. Where convection is weak and disorganized, the contribution of small clouds at and below the threshold brightness may locally be a large fraction of total rainfall.

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CAPTIONS TO FIGURES

1. Correlations between infrared cloud area and volumetric rain rate. Along the abscissa are brightness thresholds used to measure area. The ordinate indicates the time lag in hours and minutes between cloud area and rainfall. The correlation is highest for cloud area defined by a 175 dc threshold brightness and rain falling one hour and twenty minutes earlier.
 2. Same as Figure 2, but for visible clouds.
 3. Infrared clouds and cloud outlines for the four days of present rainfall estimates. The area shown is approximately the area of each estimate sequence. A hexagon marks the B-scale ship array.
 - a. 1300 GMT 4 September.
 - b. 1330 GMT 5 September.
 - c. 1330 GMT 9 September.
 - d. 1315 GMT 18 September.
 4. Time series plot of 4 and 5 September one hourly rainfall estimates over the master array (a disc of radius of 204 km centered at 8°30'N, 23°30'W). The dotted line represents satellite rainfall where the contribution of very large clouds is allocated according to the fraction of cloud intercepted by the master array.
 5. Scatter diagram of radar and satellite rainfall for 4 and 5 September. Diagonal line is of slope 1.
 6. Same as Figure 3 for 9 September.
- B-1. Infrared and visible SMS image pair annotated with cloud type.
- B-2. Frequency distributions of rain rate, for each of the seven cloud types. Dots represent gage measurements, bars represent radar measurements. Zero rainfalls above 20 occurrences have been plotted to the left of zero.

INFRARED

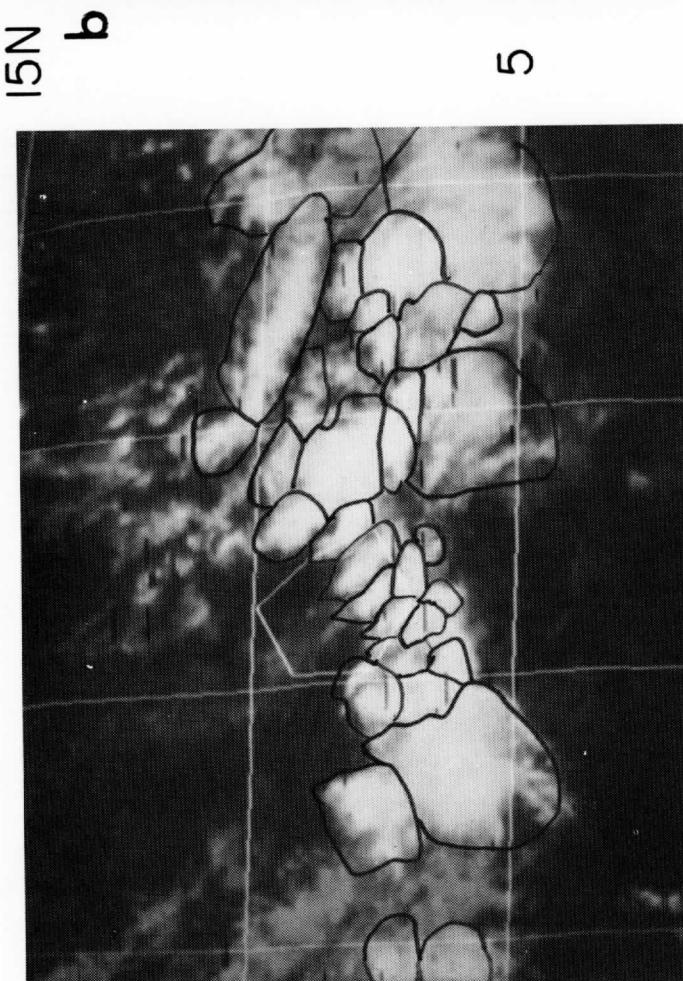
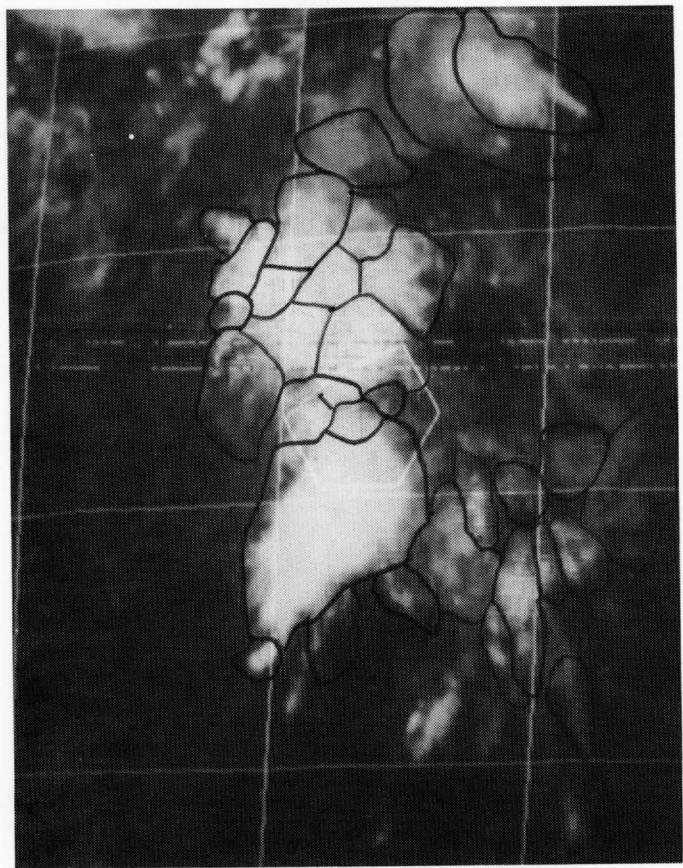
LEVEL LAG	HHMM	CORRELATION COEFFICIENT							
		100	115	130	145	160	175	190	205
-120	.5906	.6266	.6570	.6902	.7234	.7567	.8155	.8355	
-100	.6265	.6612	.6915	.7232	.7539	.7850	.8303	.8253	
-40	.6643	.6975	.7276	.7585	.7831	.8118	.8466	.8133	
-20	.7078	.7351	.7646	.7942	.8202	.8405	.8631	.8051	
0	.7425	.7723	.8000	.8278	.8511	.8674	.8796	.8069	
20	.7674	.7941	.8238	.8501	.8720	.8852	.8884	.8224	
40	.7904	.8178	.8444	.8694	.8894	.8989	.8936	.8366	
100	.8085	.8340	.8595	.8829	.9003	.9059	.8926	.8399	
120	.8224	.8456	.8699	.8911	.9055	.9175	.8867	.8285	
140	.8311	.8511	.8729	.8910	.9022	.9002	.8741	.8097	
200	.8346	.8512	.8699	.8847	.9023	.8864	.8576	.7844	
220	.8332	.8468	.8628	.8742	.8778	.8684	.8374	.7534	
240	.8274	.8383	.8520	.8602	.8601	.8483	.8133	.7214	
300	.8174	.8259	.8377	.8432	.8401	.8268	.7916	.6965	
320	.8075	.8146	.8252	.8286	.8237	.8066	.7713	.6944	
340	.7743	.7973	.8061	.8042	.778	.7800	.7407	.6939	
400	.7681	.7726	.7787	.7750	.7624	.7419	.7120	.6890	
420	.7330	.7367	.7419	.7368	.7217	.7002	.6789	.6749	
440	.6644	.6666	.6716	.6670	.6515	.6318	.6188	.6296	
500	.5702	.5715	.5790	.5780	.5652	.5493	.5438	.5709	

Figure 1

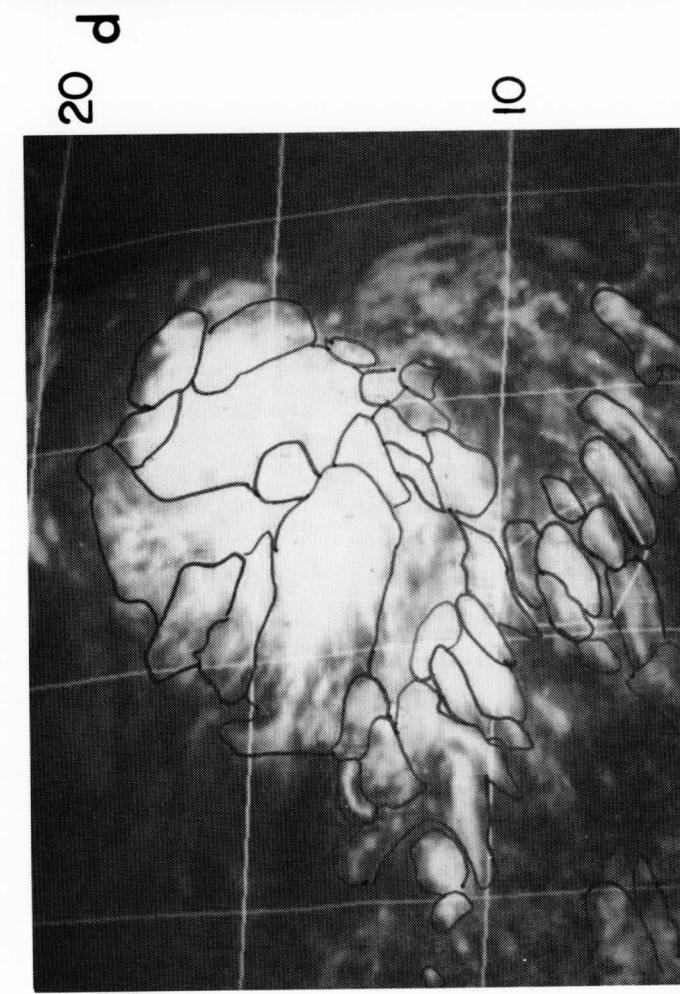
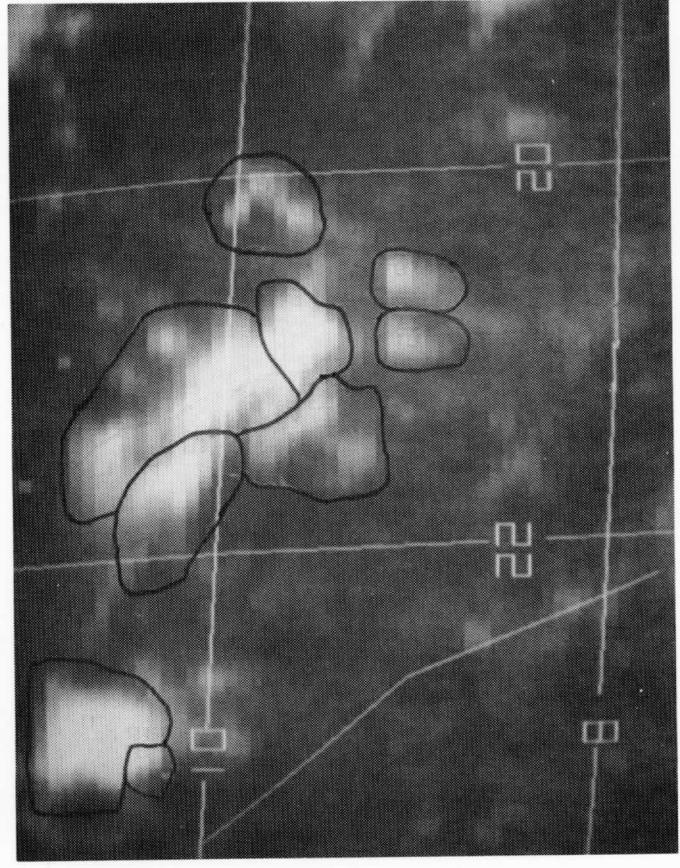
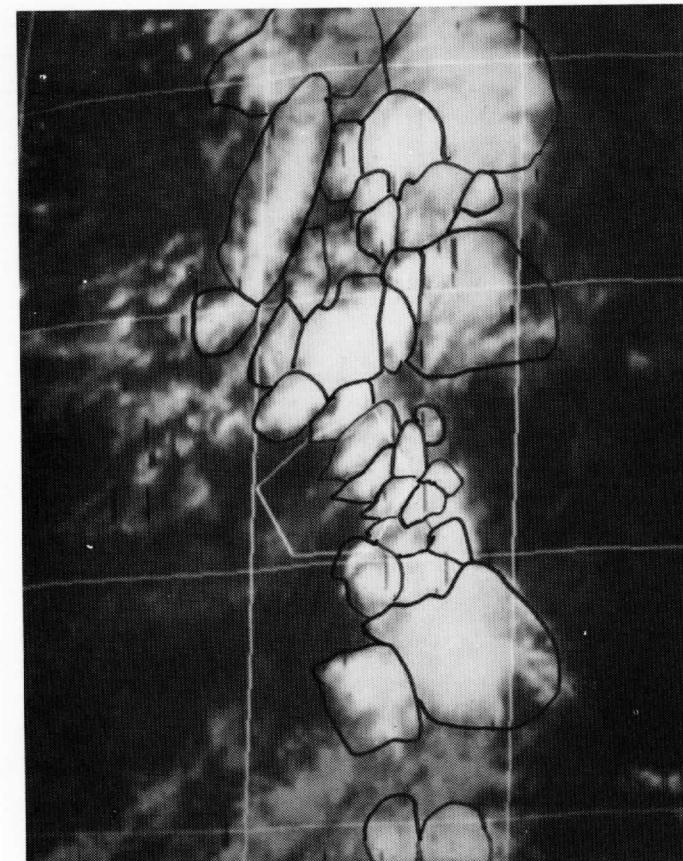
VISIBLE

LEVEL LAG	HHMM	CORRELATION COEFFICIENT							
		132	156	172	184	196	204	208	212
-120	.2875	.3171	.3476	.3773	.4070	.4267	.4379	.4502	
-100	.3877	.4219	.4554	.4865	.5156	.5335	.5427	.5539	
-40	.4911	.5294	.5651	.5975	.6237	.6395	.6461	.6551	
-20	.5905	.6311	.6669	.6983	.7104	.7319	.7531	.7421	
0	.6747	.7146	.7479	.7757	.7922	.8001	.8041	.8081	
20	.7297	.7694	.8002	.8260	.8390	.8440	.8446	.8507	
40	.7785	.8159	.8427	.8626	.8698	.8713	.8699	.8737	
100	.6121	.8454	.8660	.8776	.8774	.8752	.8706	.8708	
120	.8281	.8544	.8671	.8726	.8654	.8578	.8500	.8462	
140	.8277	.8452	.8487	.8478	.8341	.8208	.8085	.7901	
200	.8048	.8138	.8099	.8029	.7846	.7671	.7516	.7345	
220	.7587	.7603	.7522	.7380	.7131	.6974	.6756	.6553	
240	.7906	.8007	.8145	.8520	.6209	.5975	.5773	.5516	
300	.6176	.5982	.5757	.5447	.5079	.4782	.4556	.4272	
320	.5215	.4902	.4612	.4211	.3783	.3429	.3188	.2886	
340	.3872	.3464	.3120	.2646	.2187	.1770	.1533	.1215	
400	.2415	.1950	.1570	.1041	.0587	.0132	.0057	.0350	
420	.1278	.0786	.0415	.0167	.0599	.1021	.1150	.1435	
440	.0959	.0447	.0100	.0539	.0978	.1364	.1396	.1725	
500	.0622	.0143	.0140	.0730	.1144	.1451	.1412	.1823	

Figure 2



20W
30



c

Figure 3

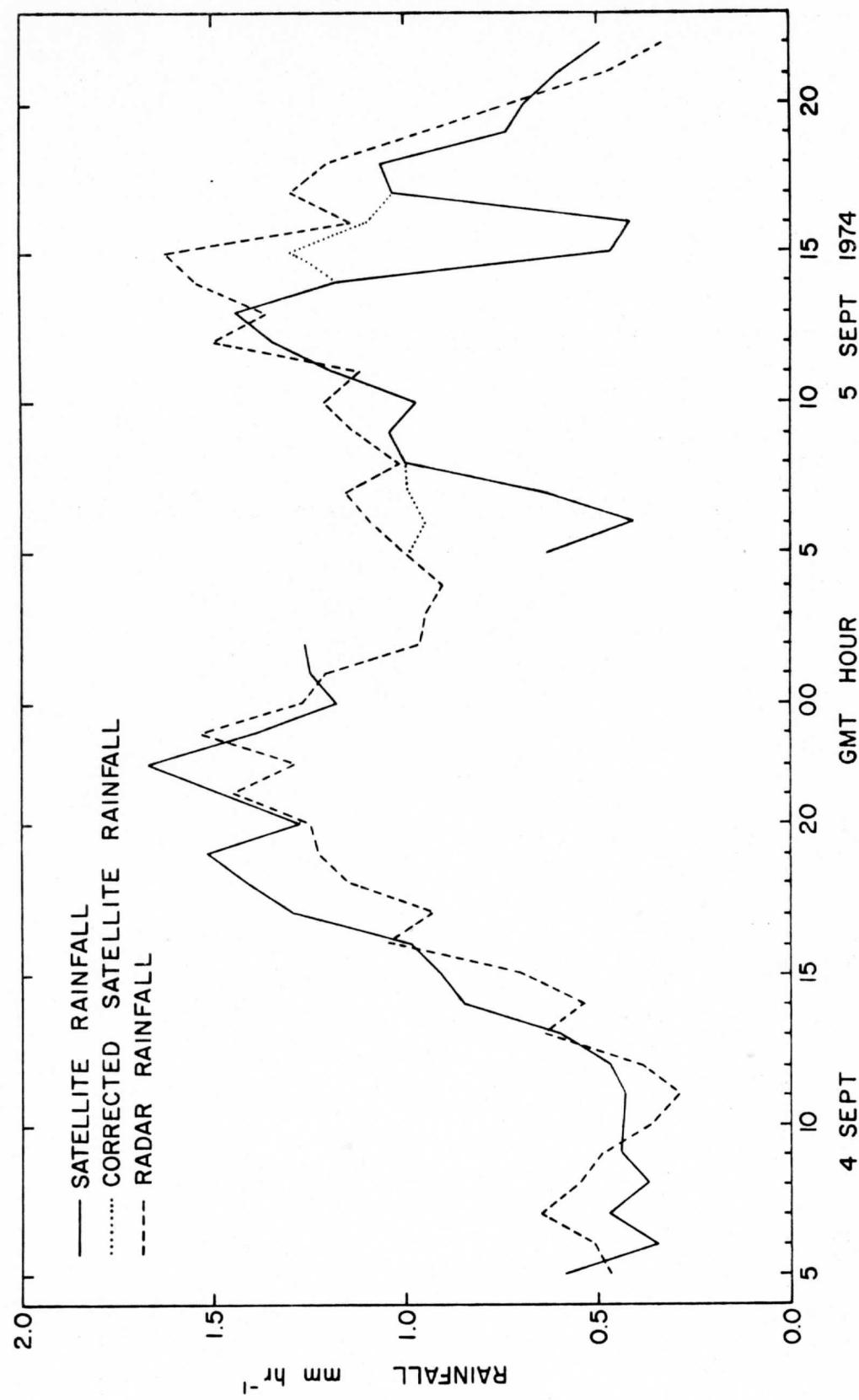


Figure 4

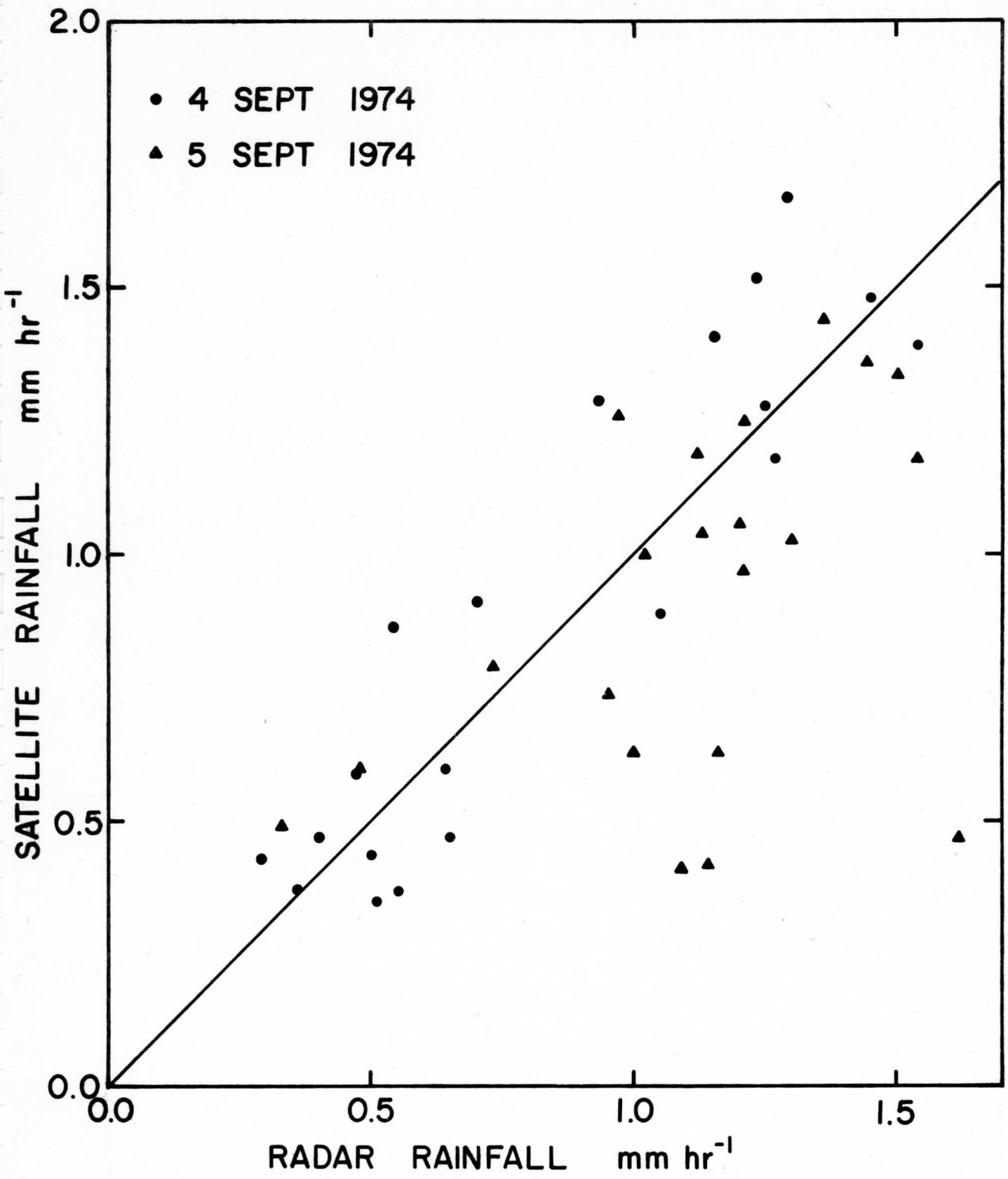


Figure 5

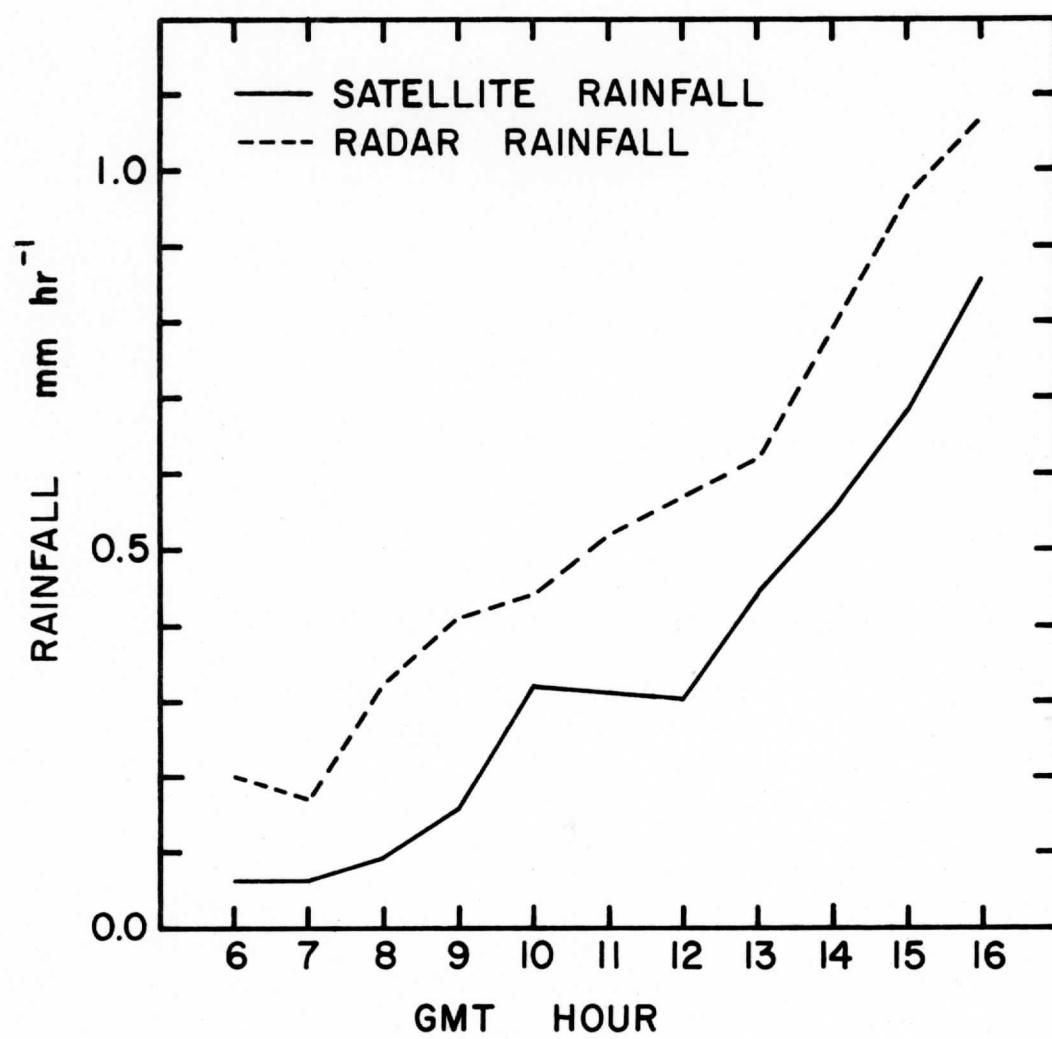
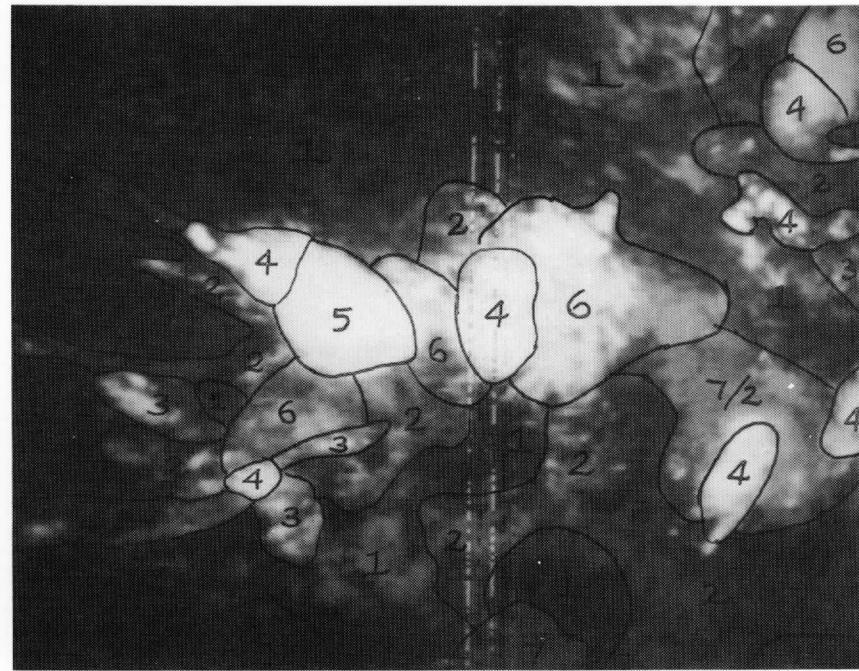


Figure 6

INFRARED



VISIBLE

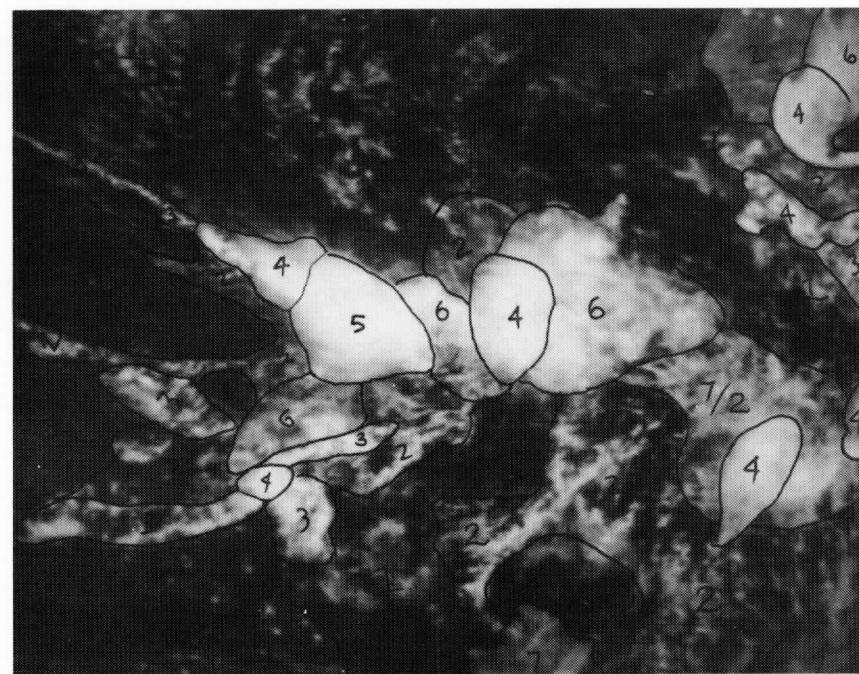


Figure B-1

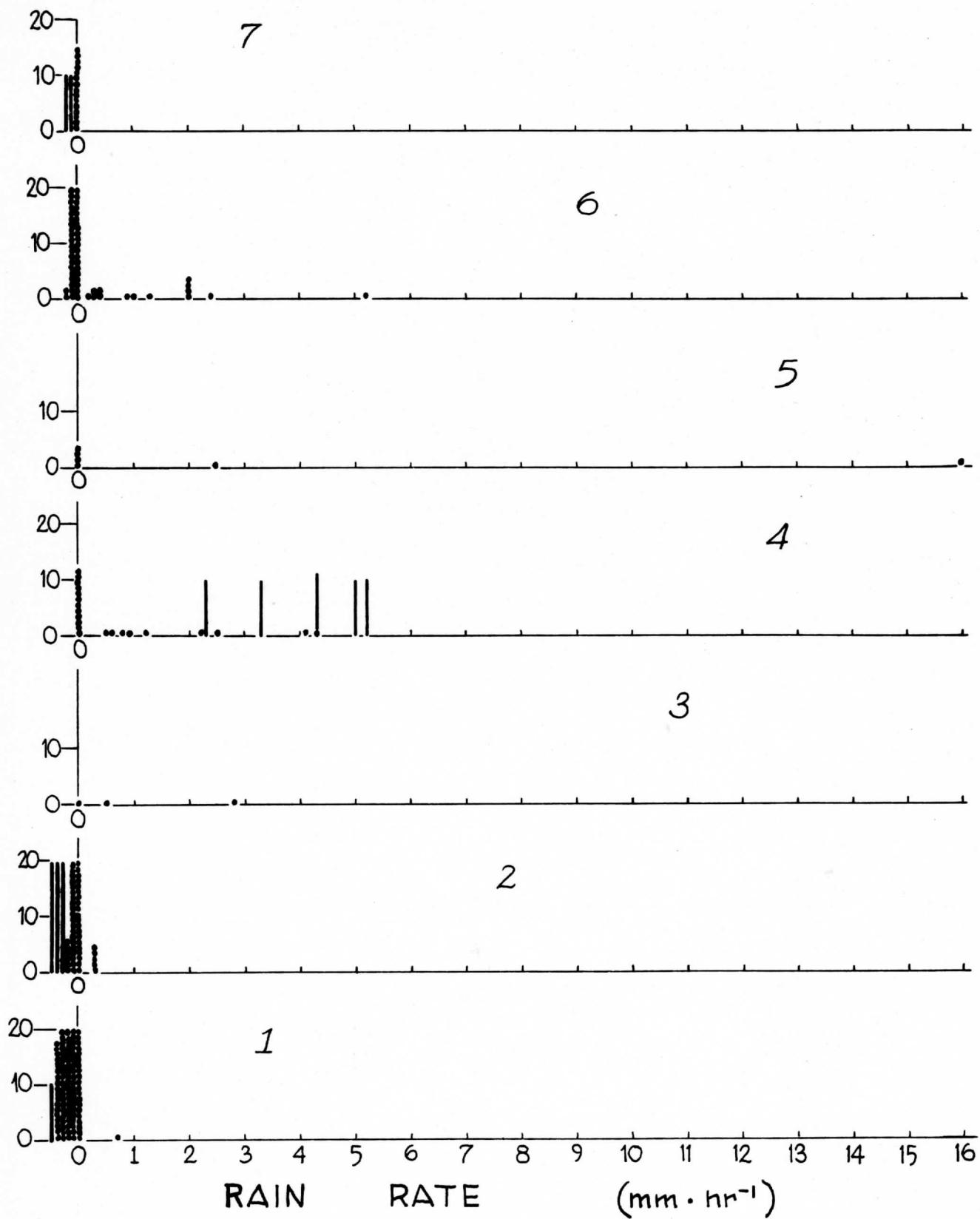


Figure B-2

APPENDIX A

Oceanographer radar data supplied by the Center for Experiment Design and Data Analysis, NOAA, had been corrected for energy loss to the sea by a "bi-scan maximazation" procedure described in Hudlow et. al. (34). The radar data were corrected for "instrument bias" and attenuation at Wisconsin. Instrument bias was removed by the addition of 2.75 decibels to the reflectivity values. Attenuation due to oxygen and water vapor was corrected by a range dependent term linearly interpolated from the following table:

distance from radar (km)	0	10	30	50	70	100	150	200	256
convection term (dbz)	0	.225	.75	1.2	1.55	2.05	2.55	2.85	3.05

APPENDIX B

Background Rainfall

During GATE there were reports from aircraft scientists and ship radar scientists of significant rain from small convective clouds and from stratiform clouds. For example, on 31 August rain was observed falling from cumulus with tops as low as 2.3 km (35). On other occasions (e.g. 18 September) heavy showers fell from congestus clouds. The echo climatologies of Houze and Cheng (36) and Lopez (37) indicate that the contribution of small, shallow convective echoes to total rainfall in and around the inner hexagon was small, perhaps a few percent. But a single estimate of "background" rainfall for the Oceanographer radar gave results between 5 and 20%, for instantaneous measurements over an area of about 10^5 km^2 (9).

We attribute this background rain to shallow convection, that is, convective clouds not reaching the stature of cumulonimbi, and to stratiform cloud not originating in deep convective clouds. It is clear from comparisons with aircraft photographs (e.g. see Simpson, 38) that these clouds can be identified in satellite picture sequences. The problem is to estimate in some simple way the amount and distribution of rain falling from such clouds.

Initially, we proposed to use cloud brightness thresholds to estimate background rainfall (9). This approach failed because the thresholds appropriate for identifying small, shallow convective clouds were extremely sensitive, especially in infrared, to other clouds, such as cirrus, not connected to the rainfall. To avoid this problem we developed a scheme which is based on a satellite convective code (39). The satellite convective

code, in turn, is an extension of the convective code proposed by Garstang, and Aspliden (40), and used by shipboard scientists during GATE.

In the original satellite convective code there were six categories, ranging from extremely depressed convection through strongly enhanced convection and post convection. The present scheme adds a seventh category of non-convective middle-level stratus cloud. This was often observed in the GATE area, especially along the equatorial fringe of the Intertropical Convergence Zone.

The revised satellite cloud code, presented in Table B-1 and Fig. B-1, includes for completeness categories of deep convection (4, 5, 3D, and to some extent 3) which ordinarily would be handled explicitly by the primary scheme for convective rain estimation. The appearance of the scene for each category is described separately for visible and infrared images. Either visible or infrared images could be used to determine cloud category; however, results are best if visible and infrared are used together.

To find out what rainfall rates are associated with these categories, clouds at the locations of GATE ships reporting one hourly rainfalls were assigned to one of the seven categories. In most cases three half-hour visible and infrared satellite picture pairs were used to make the assignment. Intervals of rapid change in cloud type were not included. Observed hourly rainfall rates then were tabulated for each cloud category, and plotted as frequency distributions. A similar procedure was followed for the C-array triangle, an area of 4075 km^2 defined by the ships Meteor, Planet, and Dallas, for which Quadra radar measurements of rainfall rate

have been provided by Geoff Austin of McGill University. Using the gage-radar comparisons made by Woodley, et. al. over south Florida as a guide, each of the C-array measurements was conservatively weighted to equal ten gage measurements. When gage and radar results are so combined (Fig. B-2), we find that there is a systematic change in rainfall rate by category. The background (non-deep convective categories) 1, 2, and 7 produce practically no rainfall. Category 3, which is transitional to deep convection, apparently produces significant rain, but occurs so infrequently that for most applications it can be ignored. The deep convective categories 4 and 5 do produce significant rainfall, however, these are accounted for explicitly by the area method; so too with the decaying category, 6. The overwhelming bulk of rainfall in the tropical east Atlantic comes from cumulonimbus clouds. Where these are small and scattered, background rainfall may contribute a large fraction to total rainfall, but where estimates include numbers of cumulonimbus clouds, background rainfall can be ignored.

TABLE B-1
A Satellite Convective Code for Estimating Background Rainfall

CODE/CONDITION	APPEARANCE IN VISIBLE	APPEARANCE IN INFRARED
1 strongly depressed convection	<p>Predominantly</p> <ul style="list-style-type: none"> • clear (black-except in sunglint) • scattered very small to small cellular clouds (cu). • patches of cloud (sc); regular spacing, low or moderate brightness • sometimes with thin, partially transparent patches and bands of layer cloud (as, ac), rapid changes in form, or • thin, veil-like layer clouds (ci), usually fast moving 	<p>Predominantly</p> <ul style="list-style-type: none"> • clear (dark) • dark-couds not visible • dark-may be faint cloud patches sometimes with • amorphous patches and bands of cloud of moderate brightness, steady or decreasing in area, dark between clouds, rapid changes in form • amorphous patches and bands of cloud of moderate brightness, usually fast moving
2 slightly to moderately depressed convection	<p>Predominantly</p> <ul style="list-style-type: none"> • many small cellular clouds (cu), often in lines and bands • bright cloud patches (sc and embedded cu), often in bands, sometimes almost solid canopy • sometimes with thin, partially transparent patches and bands of layer cloud (as, ac), or • thin, veil-like or fibrous layer clouds (ci), usually fast moving 	<p>Predominantly</p> <ul style="list-style-type: none"> • dark, small, faint clouds, seen most clearly in loop sequence with enhancement • faint but extensive cloud patches and bands sometimes with • amorphous patches and bands of cloud of moderate brightness • amorphous patches and bands of cloud of moderate brightness, usually fast moving
3 slightly enhanced convection	<p>Predominantly</p> <ul style="list-style-type: none"> • small to middle sized bright cellular clouds (cu and cg), often in lines or small bands sometimes with • chaotic patches and masses of layer cloud (st, sc, as, ac), of moderate to occasionally high brightness, usually fading; cells penetrating • veil-like layer clouds and plumes (ci), usually fast moving, not connected with cells below 	<p>Predominantly</p> <ul style="list-style-type: none"> • cellular or cobbled clouds of moderate brightness, in clumps, lines, or small bands sometimes with • amorphous patches and masses of cloud of lower brightness, usually fading; cells penetrating • amorphous patches and plumes of cloud of moderate brightness, usually fast moving

- 4 moderately enhanced convection
Predominantly
•medium to large bright cells (cb), isolated or in broken
or in broken clumps, lines, or bands; plumes
of cirrus; turrets in high resolution data;
sometimes with
expansions
•chaotic patches and masses of layer cloud
(st,sc,as,ac) of lower brightness
- 5 intense convection
Predominantly
•solid, large masses or bands of very bright
cloud, turrets in high resolution data;
rapid expansion
- 6 post-convection
Predominantly
•large flat mass or masses of bright layer
cloud (cs, from old cb's), fading and
becoming...
•extensive mixture of mostly layer clouds
(st,as,ac,ci,cs); formless, indistinct,
sometimes chaotic, often broken; mostly
moderate to high brightness; fading; in late
stages may be ringed by arc clouds
- 7 layer cloud
Predominantly
•extensive flat layer cloud (as), uniform
high brightness, some breaks
•extensive flat layer cloud, uniform moderate bright-
ness, some breaks
- Predominantly
•medium to large bright cells, isolated or in broken
clumps, lines, or bands; expansion
sometimes with
amorphous patches and masses of cloud of lower
brightness
- Predominantly
•solid, large masses or bands of very bright cloud;
very rapid expansion
- Predominantly
•large flat mass or masses of bright layer cloud,
fading, and becoming...
•extensive mixture of amorphous layer clouds, multi-
leveled (usually including some bright cirrus from
cb's), moderate to high brightness; fading

Appendix C

Tables of location, cloud area, and rain estimate, organized by time. The estimate applies to the period from the time it is listed under to the time of the next estimate.

***** RAIN ESTIMATION FOR DAY 1714247 *****

KEY	CCC	RRRRR	AAA	LAT	LONG	WHERE CCC=CLOUD NUMBER RRRR=VOLMETRIC RAIN ESTIMATE IN CUBIC METER, PER SECOND LAT=LATITUDE IN DEGREES LONGITUDE IN DEGREES	WHERE AAA=CLOUD AREA ABOVE RAIN IN SQUARE KM AAA=DEGREES MM=METERS MM=MINUTES MM=SECONDS		
330002									
	8 2232	672	2	2010 ⁴	22256	9 3774	1040	10 3449	816
	83106	-280503		7164	-240022	74515	-232221	74246	-230021
3	13611	27424	11	5244	7008	12 3514	392	13 4860	816
	74018	-223818		71805	-204159	70118	-194812	62751	-180443
5	4925	3280	4	3445	8768	6 6509	9296	11 3851	24EC
	121559	-173648		111910	-175432	95548	-165928	113456	-175756
1	35438	77632	7	5762	9536	14 2978	5840		
	34200	-140518		72502	-14951	61932	-150625		
400002									
	8 2551	1696	2	17011	26688	9 1365	2800	10 1672	24E4
	84031	-280239		65515	-241707	74359	-233349	73143	-230338
3	10219	26766	11	1645	7806	12 3257	2629	13 4567	3248
	80507	-221323		70394	-202605	71514	-133522	61846	-181735
5	980	5008	4	7012	8064	6 1020	10112	1 75419	76272
	115346	-174453		105432	-173443	103502	-174152	32605	-1522C9
7	5887	5872	14	4620	5744	16 5022	28E8	32 5610	5752
	70853	-144402		63121	-154216	61327	-290033	70459	-144433
17	1757	64	18	1630	848	19 561F	4288	21 381	1248
	90811	-265433		31548	-292023	145159	-155154	131301	-174447
31	7355	2616							
	75143	-144424							
430002									
	8 3385	2592	2	19824	28112	9 738	2720	10 2848	2624
	84230	-280913		71337	-245320	73847	-233934	73758	-230241
3	9171	29446	11	2256	64CC	12 3976	3632	13 5658	46CC
	81134	-221419		70700	-203500	70331	-201100	E3600	-182000
5	909	4064	4	4468	9520	6 5666	7630	15 1161	2C96
	121324	-175722		111814	-180441	101456	-173443	1146C4	-1824C3

1	65011	95024	7	5276	12368	14	9568	6576	16	7686	4768
	93310	-143088		72345	-155935		63129	-160217		E4434	-282950
32	22789	7152	17	2442	1008	18	1535	1600	19	2386	6096
	66144	-144917		81347	-264822		62125	-292824		150022	-155817
20	2343	608	21	1463	1088	22	5522	3216	24	4208	1248
	30523	-280332		132044	-173905		110029	-180334		E2530	-173520
23	9549	6208	28	1538	400	30	4479	5536	31	8282	6516
	90320	-161636		75320	-195318		133610	-163240		E7595	-142008
36	954	144									
	83253	-203901									

500002

8	3213	3680	2	3142	30656	9	2421	2320	10	3505	3468
	84442	-282037		63705	-242112		72624	-235813		72535	-221611
3	2545	22240	11	2837	5744	12	2791	9736	13	7734	6480
	73223	-222703		7C736	-205526		71039	-200920		E3408	-182804
5	675	3360	4	5438	3152	15	1403	2112	1	45083	1C2528
	121345	-181843		112227	-162318		120354	-182425		9C613	-141320
16	6361	7568	32	47432	17520	17	2829	2048	18	2877	5600
	63505	-284012		C5408	-150125		81217	-265824		150517	-150046
20	2472	1712	21	1314	1568	22	13114	5323	24	E503	3184
	90350	-281706		132509	-17450		105894	-181708		C2138	-175648
23	9010	3600	25	3697	4112	26	6467	1376	27	3095	3840
	90000	-170000		E5326	-251225		74600	-241823		70222	-153326
28	2871	1152	29	3061	1088	30	2670	6352	31	18299	9168
	75253	-195055		72106	-190620		133645	-163814		75217	-164721
34	2939	1440	35	1993	176	36	1768	624			
	59553	-260447		83535	-271404		83615	-204235			

E30002

3	6147	4352	2	6646	26043	3	-1	2960	11	1653	5632
	83544	-262055		64316	-243024		72201	-240250		74629	-211622
12	1359	4864	13	1339	3800	5	-1	2736	1	42810	96336
	70050	-201204		E3453	-184630		120251	-182633		1CC030	-14CC57
15	3202	3203	31	47373	33320	17	1119	2932	18	1312	5520
	E3731	-264716		E3956	-150944		81121	-271500		15C720	-155945
20	652	2560	21	575	1824	22	1926	14224	24	7430	5308
	90024	-262614		133416	-115721		103942	-175303		C3036	-181147

23	1905	11696	25	24352	-8208	26	10815	-9512	27	83C5	44CC
	92451	-17008		64138	-254615		74939	-242740		70232	-193212
28	1258	2384	29	3533	2432	31	12608	16480	34	4425	2624
	30102	-200958		71357	-191920		73356	-141502		55214	-255911
35	4483	1216	36	409	1408	33	5201	4224	48	5061	2288
	32254	-211545		84916	-205634		62153	-10122		70800	-162553
37	2378	672	38	1419	32	39	4521	3776	40	622C	1296
	82937	-301056		94107	-282445		31641	-163256		94824	-172044
41	2686	5024	49	593	1856						
	105305	-165938		131409	-170618						

600002

6	6292	6432	12	1522	4496	6	95054	-185600	15	121245	-131605
	8195	-283208		70017	-195920						
1	58140	55552	7	-1	2502	14	-1	2272	16	8278	1086
	10026	-122018		73319	-155417		65953	-165332		63304	-285753
32	65361	53264	17	-1	2720	16	-1	528	19	1233	480C
	62702	-152533		75540	-272141		32C55	-236119		152212	-154658
20	1429	2160	21	922	1600	22	9191	11072	24	5837	61EC
	35321	-234255		134033	-180703		111719	-183324		62817	-1758C9
23	3258	9280	25	14472	19120	26	11984	9104	27	11	7646
	32314	-175434		55146	-254247		74543	-243338		71145	-134439
28	139	2368	29	6409	3648	31	5527	18512	34	3796	4272
	80618	-200054		70743	-192349		75232	-150026		55146	-254247
35	7425	3312	48	910	4384	37	1046	1776	38	27E8	8CC
	93017	-272214		65453	-165932		83636	-301026		94033	-282333
39	5139	5136	40	3384	4320	41	3350	7936	42	6749	4224
	91504	-164533		93055	-172534		104140	-172505		55543	-233343
43	5024	2564	44	3322	1392	45	1716	36	4E	4095	1472
	64739	-235643		71353	-230435		81417	-204843		74643	-135613
49	861	1632	50	1567	5824	51	2725	5488	52	3237	E4C
	132833	-171222		105536	-183643		92445	-1E0135		65391	-263327
55	7112	1488									
	61300	-181920									

630002

8	9601	9072	2	5425	12752	3	-1	2160	11	757	2592
	84714	-281632		63809	-244230		72312	-222600		70710	-205715

13	-1	4576	4	411	3792	1	19162	39136	16	8519	12268
	61816	-165906		114815	-185833	1	101015	-145220		61616	-290557
32	63364	73312	20	-1	2304	22	9271	12832	24	7166	8944
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90	4793	3360	91	2254	768	92	13243	6080	93	31C9	2070
62327	-274612	55838	-173012	75047	-275703	74850	-215536				
1430002											
1	-1	1616	32	12481	54432	25	4282	58992	33	-1	21C4
101503	-152322	54313	-164029	52826	-260522	70925	-184147				
40	1267	4240	51	6848	1512	55	-1	10560	56	8C74	9552
111607	-203908	101503	-190038	61623	-194935	73103	-275117				
E5	-1	1776	69	3068	15472	71	2374	7264	72	64C6	16182
74710	-241616	65458	-30452	92523	-222305	82250	-212008				
74	7171	7166	75	3650	6112	76	5392	5964	78	7318	16396
62821	-250336	71219	-242242	72326	-231051	74428	-251242				
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30726	-184700	54251	-180743	70127	-201109	81832	-252236				
83	737	5856	84	7781	6784	85	6507	18000	86	26678	21440
74501	-234130	63914	-235417	74939	-220643	71506	-204653				
87	677	3040	88	10235	11760	89	13620	11376	90	24067	4992
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91	2185	1776	92	7573	11536	93	10296	3168	94	2935	1426
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71	572	6416	72	16193	16320	74	5635	8976	75	-1	63C4
91325	-223507	91821	-211945	55251	-249234	7203	-246031				

76	1592	7168	78	23592	16752	79	1058	3083	81	16686	13376
	72448	-231445		74405	-255430		80014	-165706		72346	-193752
83	3116	452A	84	10752	9040	85	5235	16240	86	22178	23712
	80910	-233013		62843	-240917		83544	-223852		72308	-210935
87	1385	2512	83	15152	13888	83	13495	15872	90	25310	16688
	63928	-230105		82350	-173929		83909	-162823		63757	-274556
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	60120	-173152		80550	-274247		74287	-222202		721C9	-243151
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56	-1	10240	69	-1	11456	71	1030	4832	72	3701	21568
	75315	-272206		72405	-311635		100558	-224289		80116	-214838
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	63904	-251316		71521	-230823		74929	-260032		81305	-150335
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	53003	-181244		65336	-195507		61415	-240002		64919	-2415C5
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89	14519	18263	90	29284	25616	91	-1	4320	92	12448	14304
	85204	-162427		53119	-215404		55439	-173841		81028	-268811
93	15596	12128	94	5909	5968	95	46434	22704	96	4963	2592
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	54038	-254435									

1E0000Z

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	75852	-215154		60314	-250938		79209	-234736		80952	-261728
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	81803	-190635		64728	-192445		65022	-243421		81912	-225057
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95	49620	41624	96	10223	4544	97	395	192	98	5073	3824
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83903	-214435		55332	-251659		75112	-235439		75704	-260658		
81	21414	24512	82	493	816	83	648	2608	84	6567	12422	
65039	-203642		90642	-255033		82831	-241719		62585	-243119		
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82803	-225953		71821	-214352		82057	-182325		85957	-164932		
90	28615	38496	92	13318	18768	93	23975	24224	94	634C	9E32	
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	74844	-172542										

1700002	25	15963	25072	67	5493	17584	71	2988	4632	72	2497	9840
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90225	-165152		54423	-283256		82028	-23044		74740	-224716		
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72157	-243958		65658	-172500		52635	-294924		71431	-185641		
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52318	-260259		64033	-220434		73245	-174514					

1730002	25	16417	26400	71	1035	5040	72	8037	11584	74	5775	10912
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	80027	-241258		62620	-195747		92049	-255532		91018	-234615
86	38225	44608	88	8007	14720	83	5039	20256	90	33751	50224
	65354	-212422		83304	-180711		90122	-173340		55830	-200433
92	11061	21104	93	36743	36600	94	9548	10976	95	26425	48016
	75650	-274139		83100	-223006		73239	-244449		654CC	-174C30
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	45020	-301133		65902	-188550		51333	-255725		63304	-221532
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18000002

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	92439	-260426		84901	-244603		71653	-210114		03420	-163842
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	90816	-170913		54239	-290217		73151	-231328		79356	-245159
95	4605	48288	96	3458	12192	97	476	3636	98	2550	6832
	80954	-172301		52142	-301534		70133	-185859		51339	-261216
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18100002

25	-1	22496	67	-1	6136	72	4001	14928	74	9321	8800
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90	50190	60816	92	7502	14976	93	38734	55936	94	7663	14360
	54617	-290724		83315	-282518		74934	-230427		74958	-25C10
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	69131	-174826		51750	-303034		65852	-185813		50858	-262033
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	63042	-222240		80633	-172805		82905	-290101		75449	-243039

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1900002

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2000002

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2030002

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2100002

72	-1	1968	85	-1	1128	89	2481	5136	92	-1	1600
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	73654	-260747		91328	-200019		81731	-225542			

2130002

93	40615	69672	98	1761	5696	99	1764	11760	100	1746	27792
	81646	-225548		50027	-265210		63352	-220814		73754	-175015
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	82825	-301735		82802	-135106		64803	-174213		120752	-202233
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	52326	-283326		54453	-233551		101131	-232414		50456	-300048
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	64809	-140752		70106	-260004		54046	-222402		914C4	-200341
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	82400	-175020		90229	-174049		81646	-225543			

2200002

89	-1	2096	93	43765	85536	99	3971	9248	100	5155	20528
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	53204	-234456		101369	-212735		51625	-295817		64506	-180554
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	70753	-261205		91134	-200504		83619	-140124		90311	-174850
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	81505	-230154		61537	-134051		71303	-300922			

2230002

86	-1	3056	93	43281	88208	101	1975	7552	103	2906	4896
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	E4C17	-174432		52532	-285503		52191	-240121		955C3	-224622
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	51119	-300131		64428	-181151		52815	-224923		90353	-201931
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	83519	-180127		82318	-225554		52719	-172612		61353	-134615
122	1995	2320	120	1624	736	121	785				48
	71563	-302026		74202	-181845		63927				-164247

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	75926	-240746		45443	-273421		81653	-15434	51603	-291811		
107	224	6360	108	350	704	110	7300	28016	111	5660	3C72	
54223	-2358C5		105208	-242221		51041	-304557		E4242	-180835		
114	17717	19504	115	9398	10000	117	7863	7152	118	1698	1336	
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	72528	-301130		73307	-183306	64502	-252243		1C359	-222628		
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	50455	-241506										

30002	93	44497	71856	100	1740	2304	103	347	1184	104	1738	4 664
	75417	-242256		53957	-185150		80302	-19400		E5418	-172459	
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114	19784	23440	115	3916	12465	117	5351	9344	118	1934	2288	
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	73431	-163700		65025	-245909	105602	-222126		45142	-2413C2		
126	1495	608	130	1601	1072							
	82633	-225313		81627	-182036							

100002	93	35287	74976	98	594	560	101	-1	304	109	300	13376
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60412	-241141		44743	-311928		62251	-191433		E2755	-210951		
115	5014	14208	117	7854	9840	113	2774	2704	115	55536	-132611	
84924	-162752		83712	-231736		53535	-172942				320	
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	73629	-184018		62007	-163522	64914	-250053		1C5636	-223141		
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	45033	-242226		83238	-224819	81036	-181843					

1300CZ

93	34304	72126	103	-1	192	107	-1	2136	110	1622	11632
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1114	20473	30268	115	4958	12752	117	4867	11232	110	3710	3624
92637	-211239	801736	-1811905			82047	-232152		53008	-173541	
120	4405	5860	123	389	6688	125	3977	5472	126	5105	3072
13850	-184503				65613	-251915	4927	-242931	83510	-224705	
127	819	112	128	1158	144	129	2240	1120	130	4545	1872
				101921	-2321201			63259	-250513	80056	-180504

***** RAIN ESTIMATION FOR DAY 1774248 *****

KEY CCC RRRR AAA WHERE CCC=CLOUD NUMBER AAA=CLOUD AREA ABOVE RAIN IN SQUARE KM
 LAT LON WHERE RRRR=VOLMETRIC RAIN ESTIMATE IN CUBIC METERS PER SECOND
 LAT-LATITUDE IN DDDMMSS LONGITUDE IN DDDMMSS WHERE DDD-DEGREES
 MM-MINUTES
 SS-SECONDS

4000002

	2	119 ^a	106	4	1585	2802	5	134	0	6	165 ^a	1052
	10181 ^a	-242453		10292 ^a	-240503		95927	-232414		102658		-220541
7	222	84	8	375	378	9	2952	1837	10	17390	27640	
	102200	-210917		104246	-184423		91257	-133944		81341		-175023
11	2289	31E ^c	12	1189	177	13	6684	10520	14	9683	14720	
	92155	-194105		93023	-201643		81331	-205050		30412		-210414
15	701	1873	16	917	7706	17	1643	1357	18	54C9	4481	
	85102	-225123		84000	-231306		8349	-242012		85731		-249507
19	273	0	28	13	170	20	25680	56820	22	2182	1101	
	36104	-253312		101140	-252033		72954	-251902		53900		-272127
23	1104	1906	24	2697	5915	25	1901	3880	27	1733	1222	
	52001	-272106		44534	-245300		55804	-173497		64645		-163115
26	8586	7991										
	52312	-161350										

4300002

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	105317	-255345		102035	-242943		102158	-24030		100023		-234757
6	579	1647	8	211	472	9	10513	2933	10	14175	2895C	
	103331	-220624		104211	-185006		93532	-18312		23648		-181939
11	3042	3481	12	1054	776	14	13009	15670	15	1918	17C3	
	92339	-133401		92556	-204355		95033	-215458		85339		-230003
16	7218	6119	19	1132	150	28	340	127	20	25333	54C6C	
	90337	-245126		93913	-253306		101351	-252155		74702		-250633
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59	74300	-2522212	80613	-235026	85744	-231521	85744	-231521	31527	-215108		
60	109	251	119	10104	0	71126	-212508	71126	-212508			
1630002												
61	19734	21840	31	6060	23580	36	-1	0	41	85266	112600	
62	101202	-233036	102202	-195345	55305	-274115	55305	-274115	100056	-274000		
63	-1	0	44	264	58	49	17501	20790	46	1274	23460	
64	112940	-200420	7258	-256759	80745	-205839	80745	-205839	30641	-212321		
65	711	3488	51	1447	16170	56	-1	0	58	5193	5855	
66	54028	-263552	44605	-171352	103223	-285142	103223	-285142	50513	-270609		
67	644	395	62	4075	3055	66	95	1342	67	1136	150	
68	62422	-254003	55051	-252417	42617	-255652	42617	-255652	61015	-202419		
69	7539	11190	69	1998	1152	75	799	91	73	292	0	
70	92008	-224243	65329	-292219	110602	-304447	110602	-304447	103024	-293133		
71	79	1328	1895	76	2195	3025	72	8523	77	5239	4560	
72	72640	-250627	80009	-235617	90632	-232954	90632	-232954	81246	-220007		
73	836	237	81	104756	-30121	82	87	0	119	1992	5575	
74	94337	-182026	104756	-30121	65324	-223841	65324	-223841	101127	-234356		
1700002												
75	-1	796	12	3955	26190	31	7400	29150	41	740E4	126CCC	
76	32541	-192656	93353	-222018	100423	-205708	100423	-205708	35554	-265241		
77	15141	24220	46	338	23160	51	2510	12180	59	-1	0	
78	90234	-205841	73704	-230225	50150	-171233	50150	-171233	42832	-255039		
79	3581	6968	60	840	8001	61	150	741	E3	3578	4364	
80	50323	-271404	120112	-205239	62256	-252817	62256	-252817	55314	-251040		
81	2010	1420	67	840	728	63	18388	12010	E9	1538	1905	
82	45800	-261348	55327	-203700	93551	-230505	93551	-230505	70312	-293323		

70	-1	0	75	594	502	79	226	2062	77	3993	6081
44442	-304604		110423	-305032		73211	-250852		81358	-215933	
78	1042	625	81	694	45	82	25		119	1586	4393
93949	-182716		104625	-301336		65959	-223348		55308	-235229	

1730002

12	6492	20610	31	273	21060	41	60694	129300	43	3977	25350
90923	-221908		95342	-203800		84651	-262725		63418	-212802	
46	7038	16720	48	1773	1949	51	1480	10500	58	4160	6869
80851	-224946		55514	-264517		45332	-171633		50133	-265805	
60	97	3280	63	2784	5048	66	1925	2101	67	159	973
120502	-205520		55425	-251405		45530	-262050		5596	-203647	
63	12927	18530	71	184	0	75	162	679	79	1495	1576
93233	-230824		65153	-194720		111004	-305822		7265	-245936	
76	1326	1990	72	10135	6515	77	6440	6473	78	262	1011
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91	1288	412	80	531	0	83	838	0	86	2413	0
104608	-302738		64829	-283029		52633	-245623		709C8	-293118	
85	4357	4517	119	-1	4385						
83850	-230709		94938	-240458							

1800002

12	1816	18070	41	55296	124300	43	-1	93840	-180555	44	-1	0
90709	-221339		91125	-274845		52	-1	51741	-291515	58	3585	7116
49	6106	20030	51	1051	8205	52	-1	51741	-291515	5011	-26C350	
80557	-201129		44018	-171725		66	4283	2539	63	10614	-27C544	
50	-1	2363	63	3097	5080	45537	-264102		53558	-231156		
110740	-195945		55042	-252339		81035	-234523		54156	-24C13C		
63	249	1391	79	364	1929	76	1129	2128	72	7447	10140	
65133	-293007		72247	-245056								
78	113	856	81	2049	996	82	43	0	90	533	291	
94533	-183207		104516	-303616		63741	-222705		65314	-283416		
83	521	492	87	764	0	86	910	1322	35	5493	55E8	
52641	-250032		50550	-250612		70014	-239350		83143	-224323		
90	944	204	83	1160	256							
112208	-202937		63502	-260222								

1830002

12	966	13720	41	66967	121300	49	2376	17450	46	-1	8689
	90909	-221223		84922	-270356		83025	-201105		8	80647
48	1153	1548	51	1163	6354	58	6275	6975	E1	-1	C
	53642	-263450		44833	-173492		45443	-265115		41442	-253528
63	3182	5274	65	-1	34537	0	60	3948	9131	E7	151
	55747	-250645			-154232		45454	-269743		0923	-134641
60	11506	19590	63	1038	1116	71	524	25	73	907	C
	93033	-230717		65512	-2397613		63223	-134549		102301	-101620
75	4301	1887	76	395	2446	72	406	11220		4735	5548
	72915	-245142		81559	-231128		91691	-232253		31942	-245953
81	2434	1624	82	56	24	83	43	632	87	1033	419
	104512	-304339		63949	-222426		53132	-245812		50823	-251256
86	1071	1375	85	2703	8930	90	1373	661	92	1286	4484
	71415	-233047		83717	-225504		111717	-203350		71740	-215802
93	1121	384	95	310	230	94	635	555			
	110034	-201811		110542	-193656		103435	-134127			

1900002

12	-1	5917	31	114230	-224627	39	-1	0	E5	556	C
	90524	-221356					62213	-191500		42050	-2818C2
51	2545	5112	58	3284	8348	66	4250	5017	E8	5254	2038C
	44333	-174102		50330	-271055		45620	-265133		93447	-230626
69	-1	1355	75	-1	0	73	1209	-497	74	-1	C
	71027	-234438		110929	-312159		102122	-301918		100429	-100557
79	3630	3685	76	-1	1939	72	-1	8125	77	241	6501
	73017	-244601		83249	-231130		32152	-240432		31953	-215544
78	-1	234	81	394	2618	80	-1	202	85	6162	E31
	93739	-183635		103207	-304643		65932	-294353		34113	-23C347
90	1538	1218	51	2033	0	92	1932	3848	83	2665	885
	111842	-204440		71926	-242056		73749	-215746		105632	-200555
95	47	332	96	1954	-19010	0	97	993	0	98	5525
	110456	-134153		105414	-190136		69001	-252312		70932	-231131

2000002

61	1227	58900	48	54505	-264115	55	2971	541	E1	1655	49C7
	83539	-263101					91726	-283313		91442	-190234
66	6557	6488	67	-1	0	69	3169	14930		73	2215
	50332	-265213		52912	-213106		91916	-233239		100349	-301316

79	2056	5251	81	10454	1645	82	-1	24	83	-1	5357	0	
85	10977	8970	89	683	0	88	-1	0	91	2581	1341	-24C427	
85	85004	-225454	42706	-243134	65337	-255734	71555	-24C427	71555	-24C427	71555	-24C427	
93	2302	2973	94	4895	76	97	9806	4716	98	6596	7313	-231427	
93	103945	-203920	102207	-154843	71243	-254417	72207	-231427	72207	-231427	72207	-231427	
93	14020	19440	100	18201	22010	102	1074	783	101	3889	7105	-26C544	
93	92320	-282427	83635	-272613	70606	-293567	75019	-26C544	75019	-26C544	75019	-26C544	
107	414	0	103	2137	0	104	1725	1739	104	240114	104	-240114	
107	61600	-261842	113102	-231850	109756	-240114	109756	-240114	109756	-240114	109756	-240114	
2030007													
55	4432	1735	51	1625	4363	66	2951	8161	71	6474	0	-195633	
73	41110	-283717	40304	-160906	50415	-270311	50415	-270311	50415	-270311	50415	-270311	
73	1574	2196	79	839	4824	87	181	93	85	8319	12330	-225653	
73	95753	-301233	72107	-250207	52742	-243205	52742	-243205	52742	-243205	52742	-243205	
89	26	46	91	5543	2781	93	1333	3355	95	105030	-200654	0	
89	41944	-242632	70618	-240611	104559	-210703	104559	-210703	104559	-210703	104559	-210703	
94	3444	2735	97	5755	8694	93	6601	8763	99	17673	21310	-283C38	
94	102731	-195336	70156	-255527	71917	-231049	71917	-231049	71917	-231049	71917	-231049	
100	16017	25470	102	2709	1140	101	9478	10420	107	2415	227	-27363-3	
100	84328	-272708	70005	-291950	75931	-263744	75931	-263744	75931	-263744	75931	-263744	
103	3940	1171	104	1681	2212	105	923	0	107	55653	-27363-3	-27363-3	
103	112643	-233050	105934	-2334157	45334	-250201	45334	-250201	45334	-250201	45334	-250201	
2100007													
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79	82651	-204133	41622	-283554	50128	-262832	50128	-262832	50128	-262832	50128	-262832	
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91	4013	4995	93	2508	3093	94	1447	3813	36	-104933	0	-104933	-104933
91	70235	-234823	103333	-210137	10220	-195905	10220	-195905	10220	-195905	10220	-195905	
97	2929	9275	93	13505	9187	93	13262	24730	100	17654	26710	-272824	
97	65630	-253400	72527	-230836	92550	-285820	92550	-285820	92550	-285820	92550	-285820	
102	3558	2287	101	12626	12530	107	3842	1483	103	4371	2983	-235155	
102	65417	-294318	75905	-263917	55025	-274307	55025	-274307	55025	-274307	55025	-274307	
104	5342	2435	106	230	0	105	1279	232	103	660	0	-201639	
104	105523	-235428	74850	-163847	46232	-245220	46232	-245220	46232	-245220	46232	-245220	

110 1389 527 1C9 133 53517 -212558 C

21300002

41	1937	1826C	55	2969	4716	51	211	2707	58	52431	226
31042	-264038		41003	-235316		35348	-142741		52431	-272859	
E3	-1	0	66	3000	5347	68	2102	1789	73	E46	2106
62808	-250521		50133	-261120		10349	-240136		101609	-3028C7	
86	-1	0	65	415	12620	50	1165	545	89	-1	7C
72013	-293855		75115	-224455		110341	-222901		93435	-243539	
92	-1	12	93	1364	3552	97	5859	8136	98	945C	1428C
71654	-222255		103950	-210804		70607	-258120		735C7	-232830	
99	12031	24C8C	1C0	16328	28680	102	4815	3560	101	758E	1574C
95613	-232105		84108	-273141		55113	-232121		75919	-264115	
107	1672	3145	103	4075	4435	104	1120	4641	1C5	161C	854
62115	-232308		111806	-234059		111219	-234323		44215	-245329	
106	1573	362	110	1195	1152	111	226	0	112	284	C
115721	-202310		94154	-301234		113740	-215741		62859	-292541	

2200002

55	76	4965	51	404	2033	59	-1	160	66	7C8	5761
41729	-294317		34657	-181526		54240	-272034		50433	-263416	
B1	-1	0	87	-1	0	50	738	1022	97	5367	8939
103143	-305822		51427	-241146		110496	-225309		70502	-254351	
98	11113	15240	59	6992	23970	100	10603	29000	102	3937	5145
72254	-231657		85948	-232434		84036	-274130		65123	-2903C3	
101	12446	1524C	103	1249	540C	1C6	755	777	105	2737	1ECC
75057	-265107		114311	-240359		74730	-183935		44047	-2444C2	
106	1662	1117	110	3048	1454	109	53915	-212204	111	2073	124
115447	-203226		93013	-300430					114318	-215612	
112	2785	156	62853	-232443							

2230002

E5	31	3537	51	288	1553	79	-1	1037	77	-1	215151
41944	-295322		40438	-160303		71337	-253505		81153	-215151	
E5	26	5373	91	1175	1900	97	E419	9235	98	9137	1682C
80523	-232535		64001	-240751		70206	-252310		72323	-232458	

33	19088	20710	100	3143	26210	102	2663	5730	101	16341	17550
	9015€	-285437		63048	-273705		61357	-292832		75225	-265319
107	381	1588	103	364	4437	104	995	1922	106	468	
	63022	-283503		114421	-241234		110204	-243134		20553	-182877
105	2549	2626	108	1461	1807	110	1735	2694	112	2755	1625
	43748	-244156		115834	-203507		93303	-301339		2362E	-292CC4
113	2794	5232	118	660	1175	115	393	1186			
	74514	-273107		110934	-240367		54027	-212335			

230002

233002

***** RAIN ESTIMATION FOR DAY 1774252 *****

KEY CCC RRRR AAA WHFRE CCC=CLOUD NUMBER AAA= CLOUD AREA ABOVE HAIN IN SQUARE KM WHERE DDD=DEGREES
 LAT LAT MM=MINUTES
 LON LON SS=SECONDS
 RRRR=VOLMETRIC RAIN ESTIMATE IN CUBIC METERS PER SECOND
 LAT=LATITUDE IN DDMMSS LO=LONGITUDE IN DDMMSS

430002

16	5002	1090	17	7108	4063	16	9491	25150	19	12116	24770
163915	-17041	161457	-180958	153859	-194618	152752	-214824				
20	13089	7102	21	9193	16890	22	9459	17010	23	5201	1384
153859	-194618	153656	-194043	144956	-181743	141457	-203546				
24	7961	9939	25	4738	4235	26	4188	4710	13	877	749
141457	-203546	133057	-202159	134329	-212012	134457	-163220				
12	4606	4145	14	4101	3624	14	9974	43420	9	4551	6101
131723	-172858	121711	-163455	122704	-243724	122003	-205858				
10	28516	56730	11	2657	1206	11	3271	670	2	12221	15770
115036	-182849	104925	-204443	104719	-314325	72323	-291411				
3	131	0	5	2597	6507	6	4096	2153	7	9711	14300
91528	-235836	74340	-212432	74635	-203446	72635	-195841				
8	531	393									
	71606	-172708									

500002

17	8607	6755	18	19560	22910	19	7015	24080	20	11065	12500
161948	-181636	153509	-184821	153943	-211822	15325	-194850				
21	14659	16930	22	8959	17160	23	12930	3824	24	10194	11360
153314	-193057	145439	-183019	142658	-202903	14204	-204048				
25	6265	5578	26	410	5611	12	9156	5442	14	2710	4799
132057	-202001	133532	-213419	131803	-174017	121403	-164658				
4	24646	36040	9	5876	8198	10	25768	55570	11	4572	2305
122210	-243336	121958	-211337	115059	-183949	104126	-203530				
1	3770	2264	2	13569	17800	3	2302	72	5	2503	6005
85015	-313813	72104	-290243	90659	-241656	73919	-212932				
6	5126	3760	7	8664	15390	8	963	568	71229	-173019	
73843	-205138	72953	-193944								

530002

-	16	10970	7280	17	8269	9472	1P	20076	26846	19	12663	20800
-	164622	-171221		162936	-182601		1P	153632	-192930		152826	-211745
20	15650	14864	21	5165	19952	22	1C081	16992	23	11792	9776	
154138	-165351		153632	-192930		145806	-182847		143157	-203902		
24	6562	13564	25	10896	7360	26	1057	4176	12	7027	8848	
142627	-710413		132353	-202722		132809	-211607		131537	-174748		
14	4057	4564	4	37060	38680	9	7634	8992	10	20049	53248	
121543	-164936		121412	-244633		121641	-213021		114414	-184144		
11	1476	4128	1	2046	3664	2	17206	19968	3	2110	1312	
1n3417	-211420		90540	-312909		71609	-292409		85512	-243125		
5	1163	5600	6	6655	5456	7	3274	15584	8	793	928	
73527	-211503		74239	-202443		72256	-195220		70601	-174115		

600002

15	170928	-182640	16	3501	11136	17	9346	11200	16	39427	29904
			164522	-172613		160343	-184650		154302	-193714	
19	2010	21584	20	13951	19040	21	7742	16880	22	213	17488
153431	-210553		154557	-195424		154302	-193915		145035	-184717	
23	19356	13344	24	7522	14256	25	13382	11152	12	13300	10080
143401	-204324		142552	-212240		132155	-201634		132221	-174511	
14	2115	5648	4	19993	47680	9	12717	10624	10	11574	48480
121437	-165422		120706	-244407		120228	-212121		113044	-165210	
1	1476	3712	2	7776	23496	3	2563	2080	6	5387	7488
50453	-314251		71530	-292204		84818	-245208		74028	-203410	
7	2764	12768									
	71700	-200018									

630002

16	6467	9760	17	7550	13006	18	56046	42656	19	6555	16304
164149	-173419		162444	-181904		153923	-185441		154959	-214458	
20	5040	21072	21	8241	16128	23	9222	20000	24	8376	14160
155045	-201626		153234	-200159		143333	-20406		142908	-214708	
25	9718	15184	26	134447	1024	13	134713	-170218	12	17727	14384
131725	-203519			-222841						131427	-180715
14	2948	5136	4	26426	44528	9	3303	14448	10	5589	40480
120303	-170647		120923	-244933		115743	-213731		113436	-165139	
1	1580	3424	2	8252	20800	3	1818	2880	5	177	1952
90855	-314535		72357	-293441		65013	-244412		71252	-214243	

6	6573	8224	7	215	10352	8	-1	272	27	379	0
	73552	-704337		71233	-200744		64902	-175550		153253	-164300
31	8097	1232	34	2736	416	3C	4331	2268	29	2175	80
	111023	-241946		80655	-213140		141819	*185800		162533	-171918
32	1494	6010									
	1110351	-192427									

700002

16	1701	10416	17	3944	13296	1P	55161	60768	19	1449	15072
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	65553	-193628		125539	-150851		93416	-233355		65714	-173708
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89	"1	2441	97	"1	45	91	"1	4058	-210306			

***** RAIN ESTIMATION FOR DAY 1774261 *****

KEY	CCC	RRRR	AAA	WHERE CCC=CLOUD NUMBER LAT LCN	AAA=CLOUD AREA ABOVE RAIN IN SQUARE KM RRRR=VOLMETRIC RAIN ESTIMATE IN CUBIC METERS PER SECOND LATE LATITUDE IN DDMMSS	WHERE DDD=DEGREES MM=MINUTES SS=SECONDS MM=MINUTES SS=SECONDS
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	102446	-224118				
	9 804	16				
	100845	-135342				
830002						
	1 29	0	2 1151	1808 103156 -224344	3 122 100430 -224343	5 31 81017 -233725
	102452	-232723				
	7 212	2016	8 325	928 92819 -205222	9 212 100847 -200340	10 -1 105935 -201716
	9 715	-211325				
	11 407	160				
	105958	-222349				
900002						
	2 765	1904	3 240	608 95929 -224900	4 103329 -222425	5 227 81240 -234946
	103453	-224539				
	8 682	832	13 329	16 100333 -203918	14 1139 94623 -202546	
	93147	-205202				
930002						
	2 891	1760	3 156	560 95907 -225059	5 308 81556 -235056	8 489 33155 -205547
	103823	-224921				
	12 175	0	13 2557	192 95147 -204811	14 1534 94833 -202915	
	103200	-220823				
1000002						
	1 104108	0	2 608	1728 104304 -224917	11 110326 -223221	12 484 103712 -220038
	13 2560	1536	14 1340	1280 94939 -203654		
	95642	-205532				

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	80816	-230241		95940	-212301		93110	-210216		102749	-221538	
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	35940	-205958		94906	-203202		95314	-210955				
103000Z	2	139	1360	12	404	448	13	1674	2400	15	1981	464
	104515	-223100		103945	-202031		95226	-203130		5839	-211427	
104500Z	9	-1	0	13	2438	2512	14	137	1058	15	2095	978
	95808	-200403		95613	-204443		34645	-203753		100223	-212043	
	16	54	0	17	728	448						
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	75546	-241106		100941	-204317		94437	-204137		100738	-212315	
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	102754	-223624		93720	-211055		100426	-223615		102709	-225132	
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	103406	-225706										

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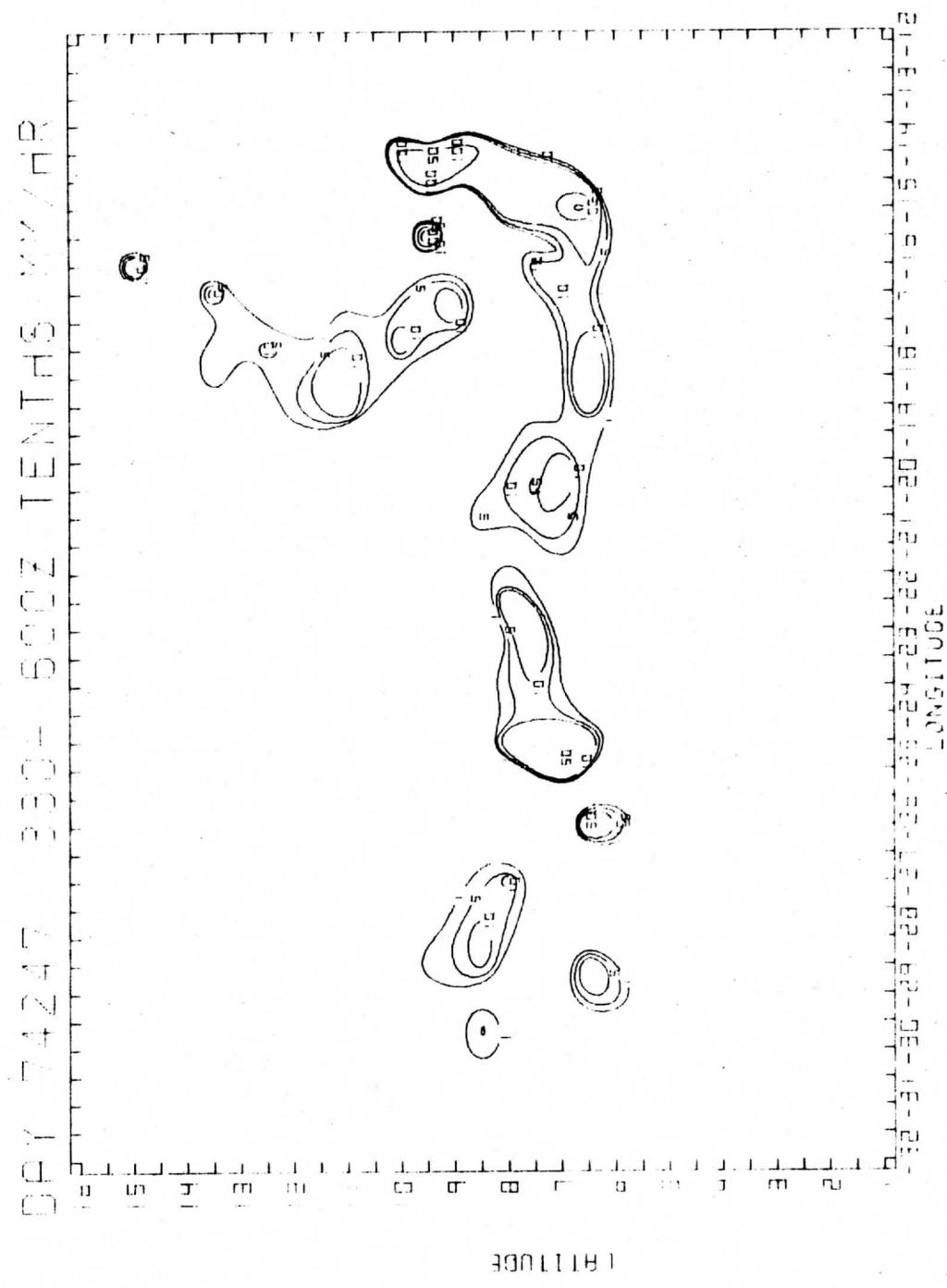
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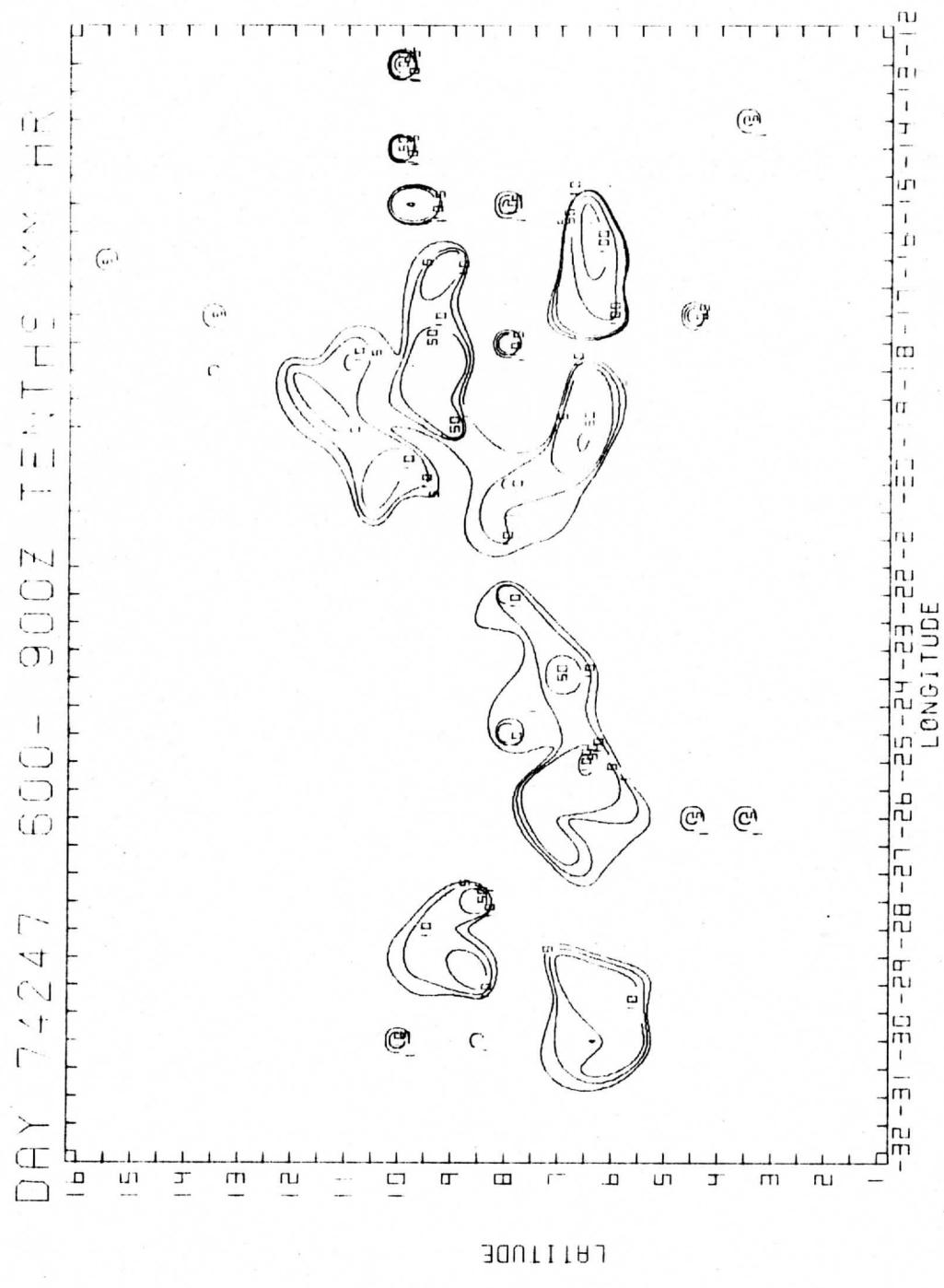
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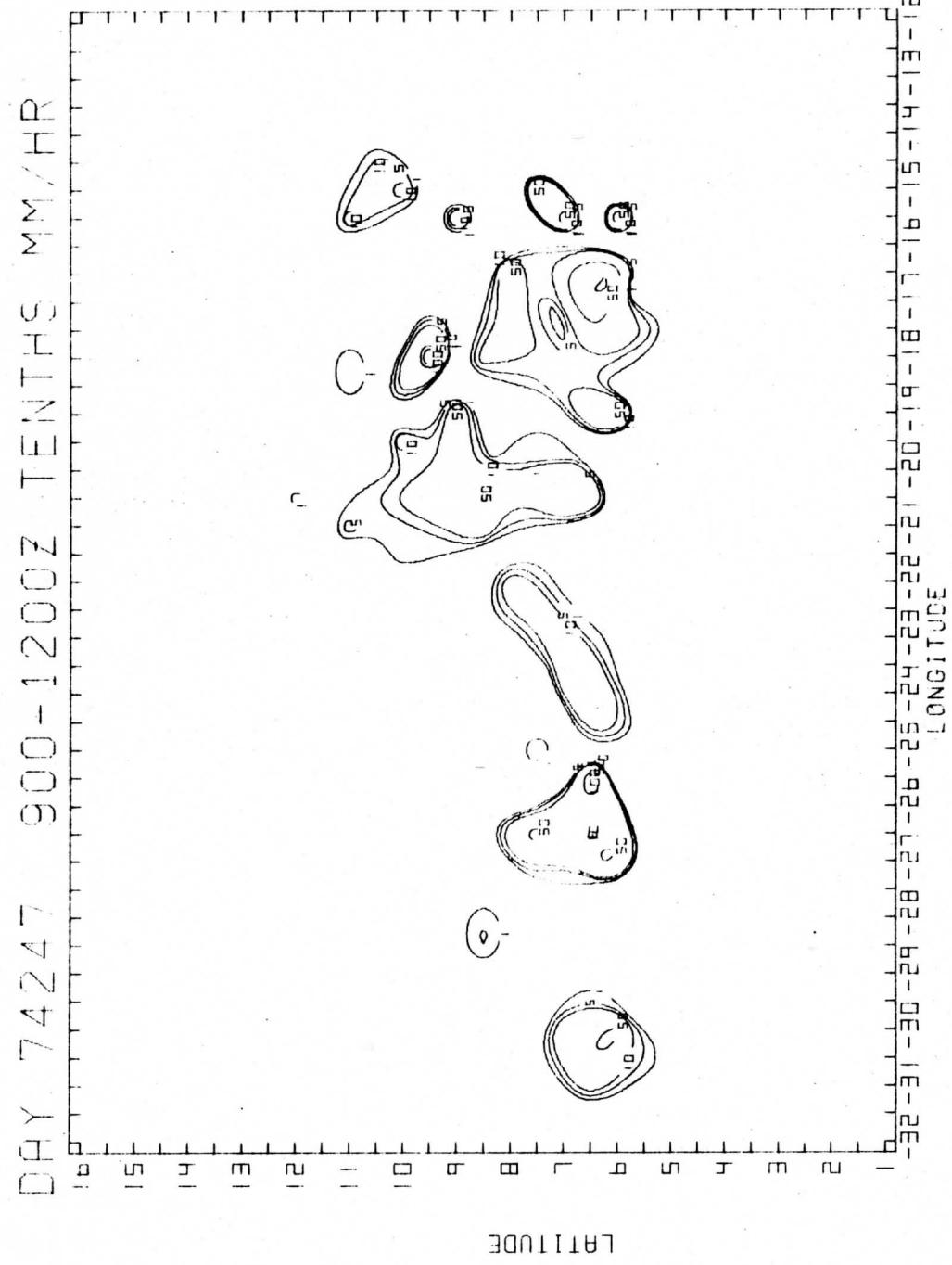
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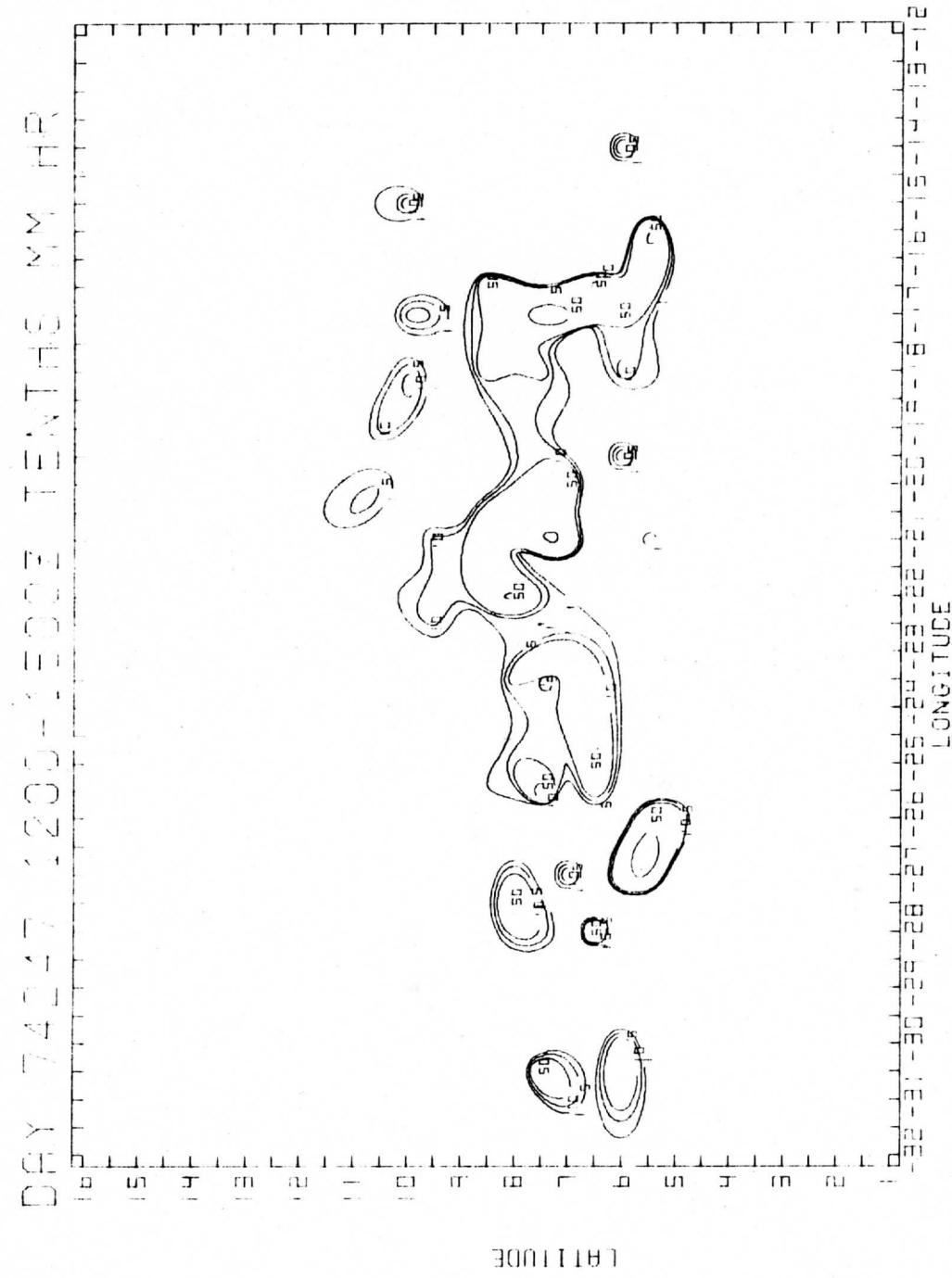
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Appendix D



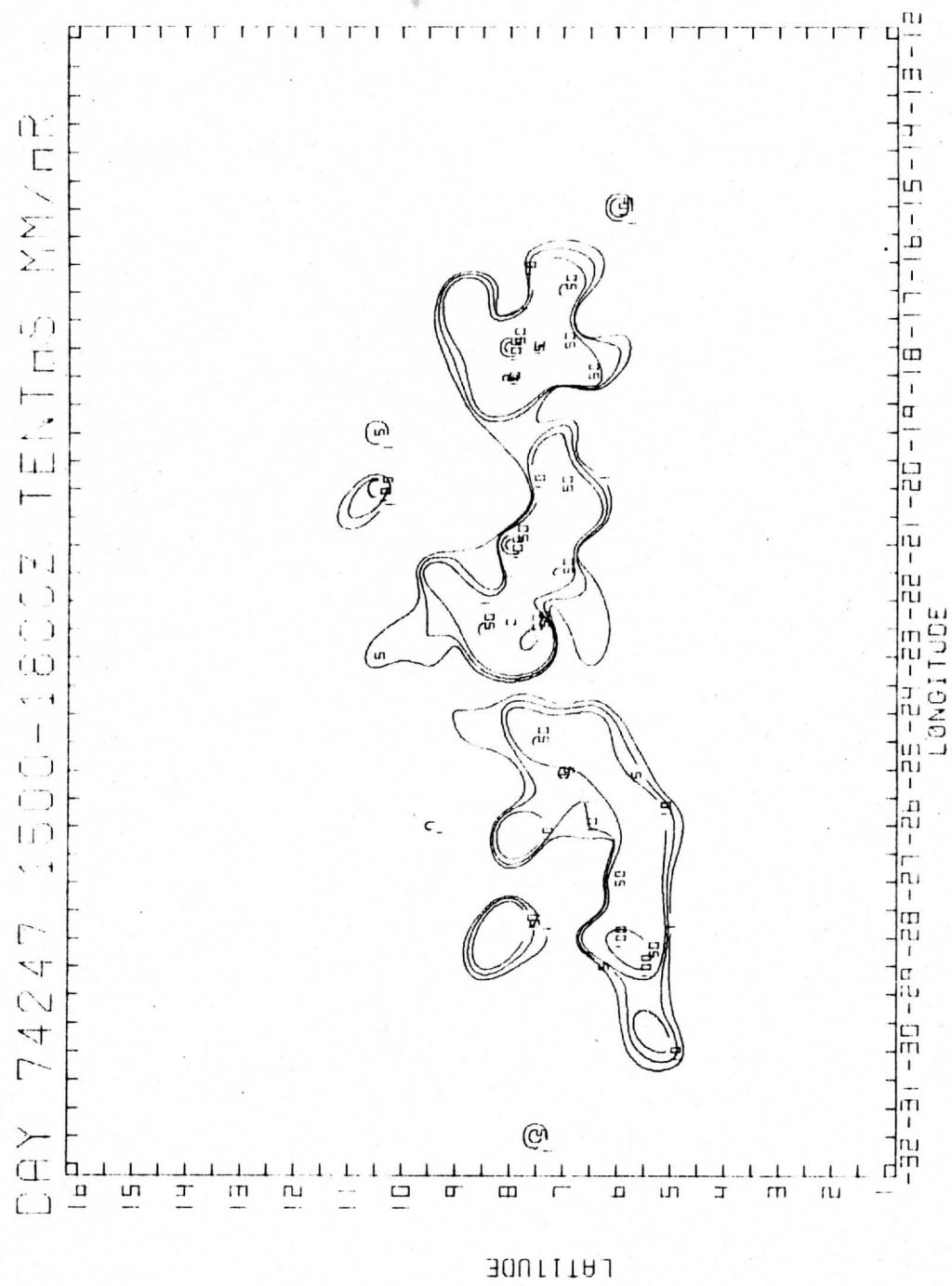


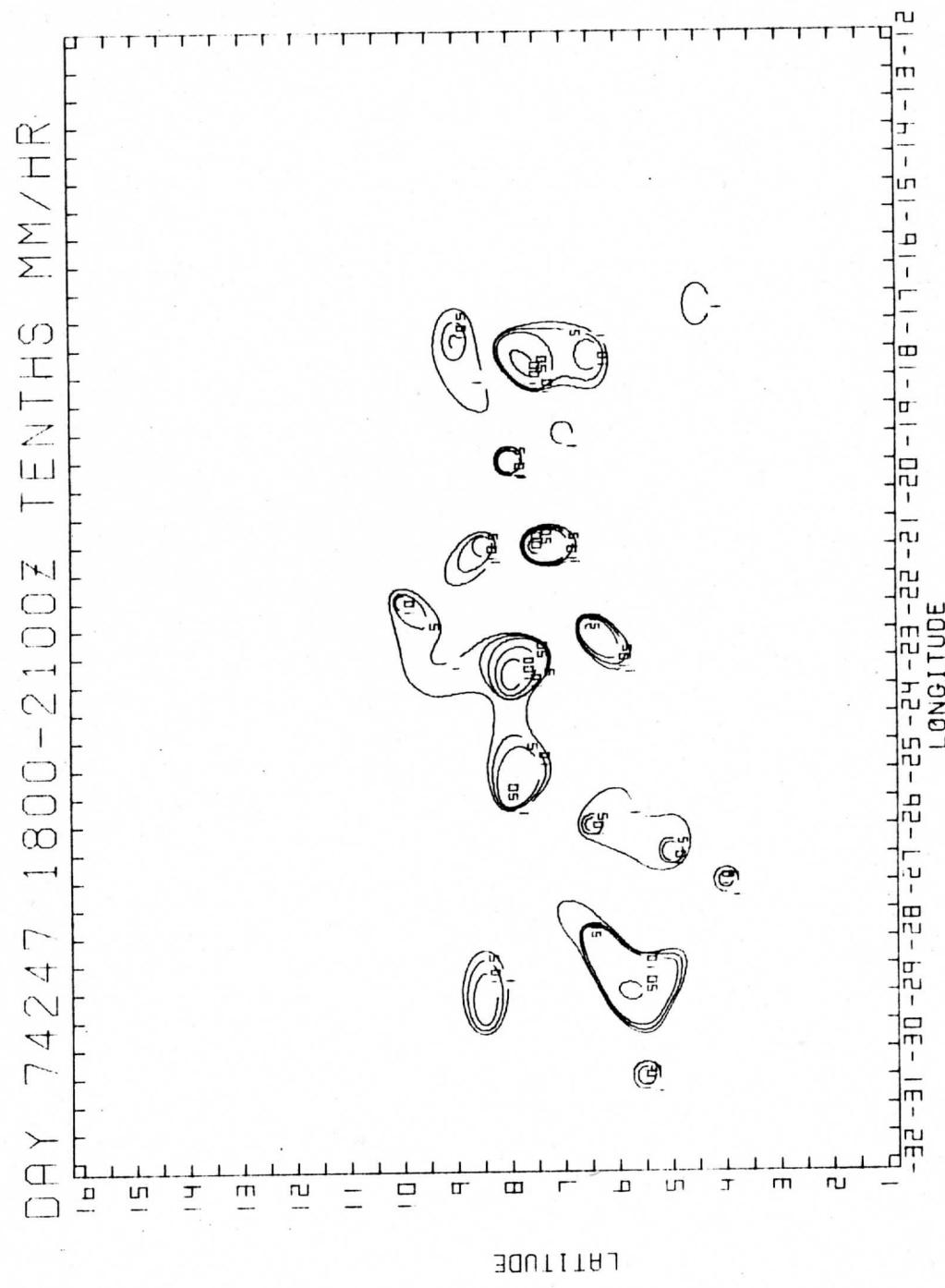


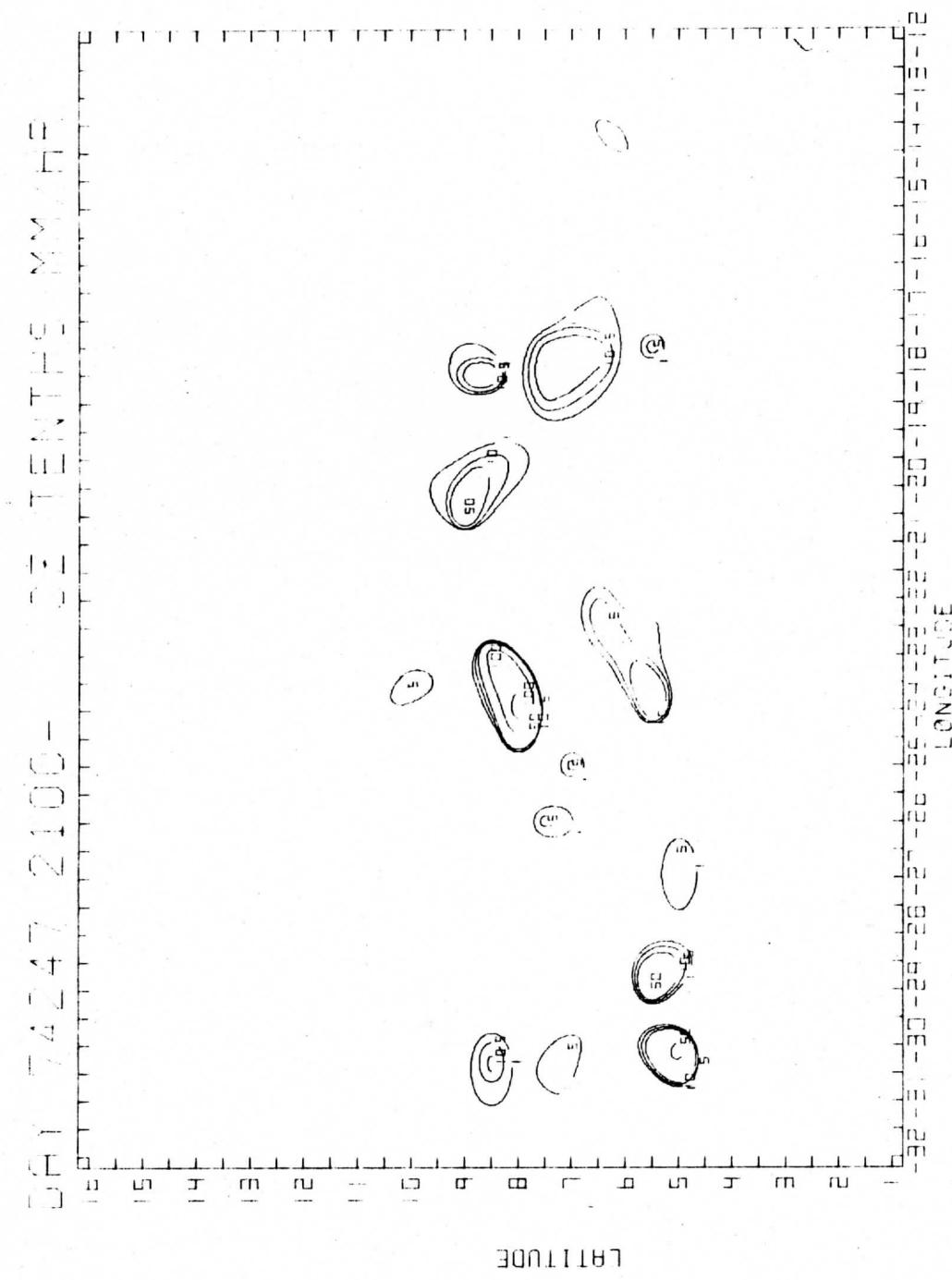


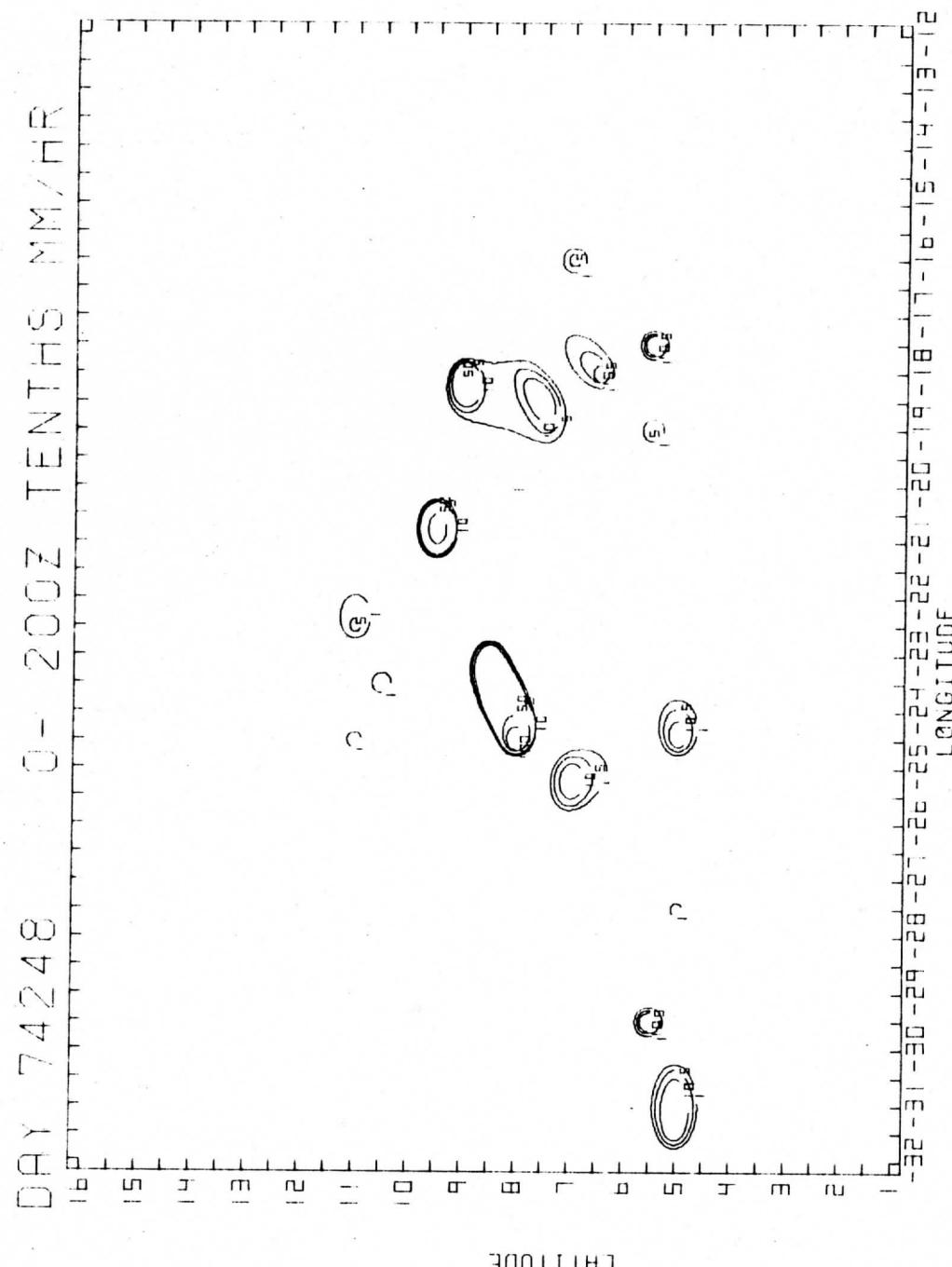
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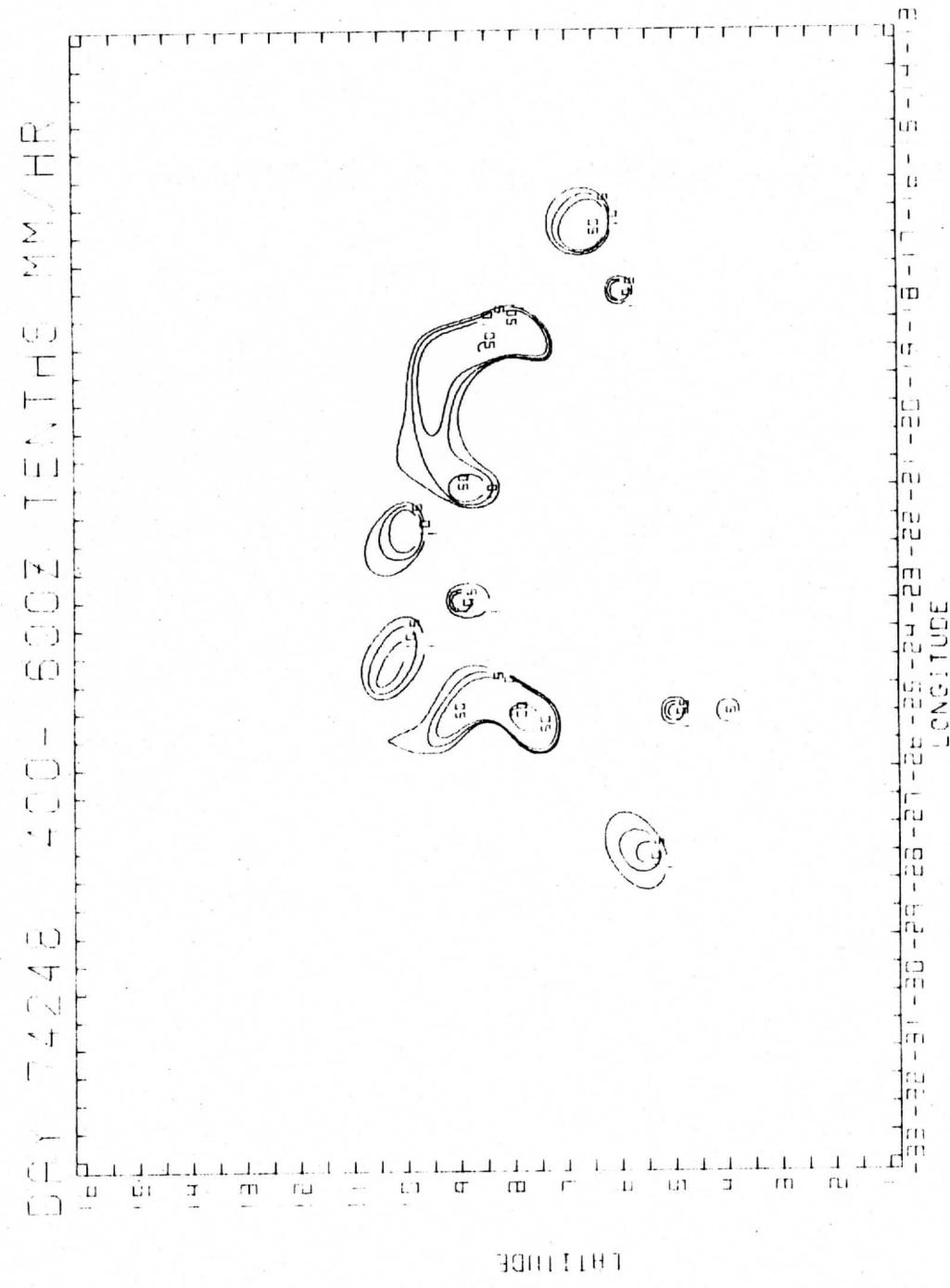
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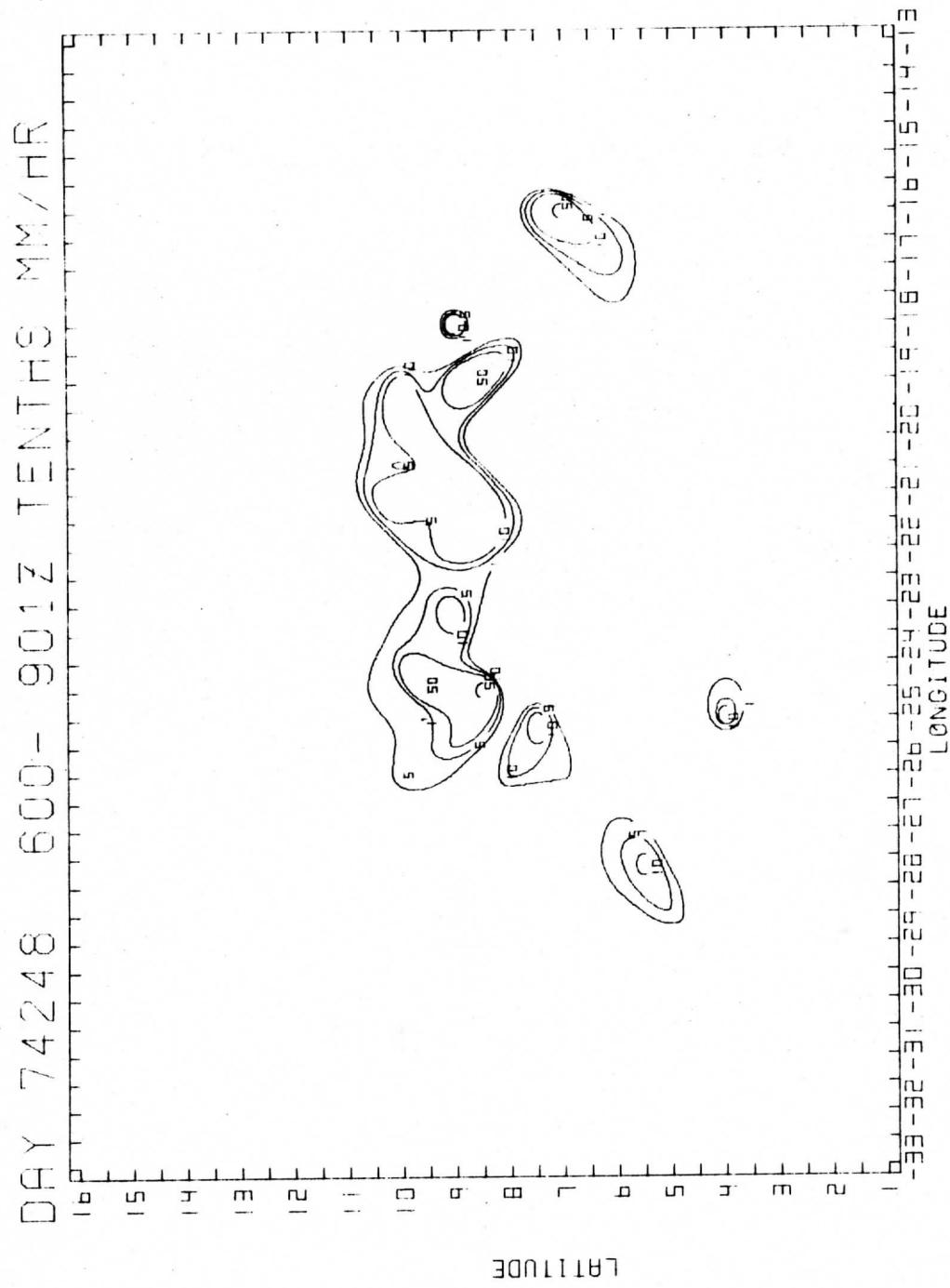


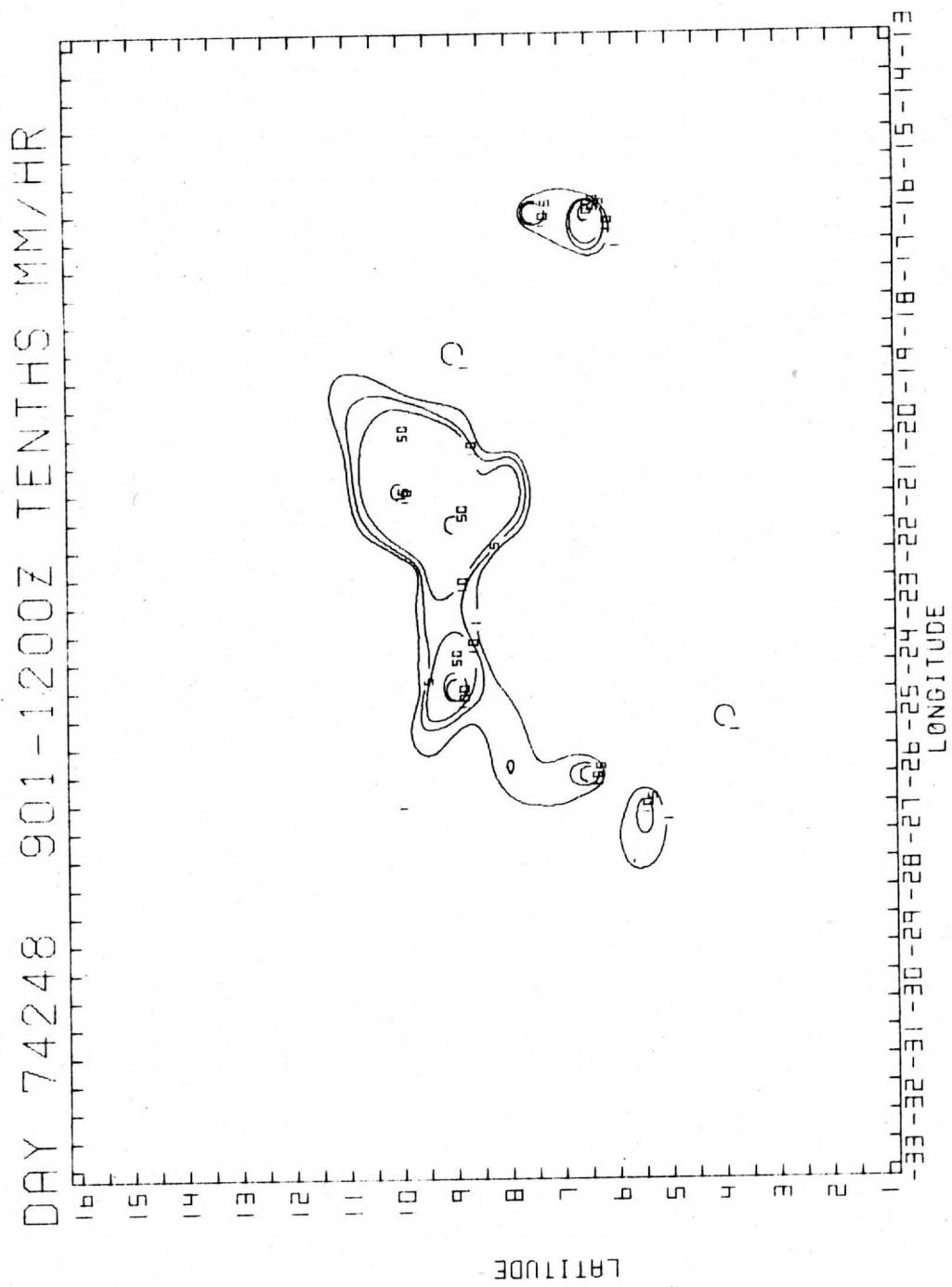












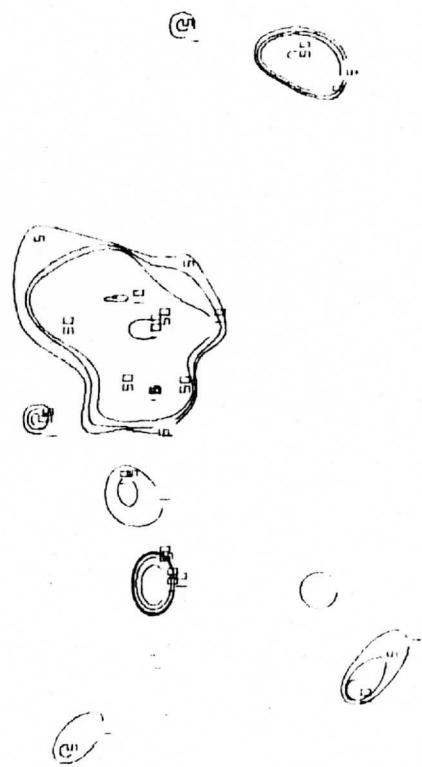
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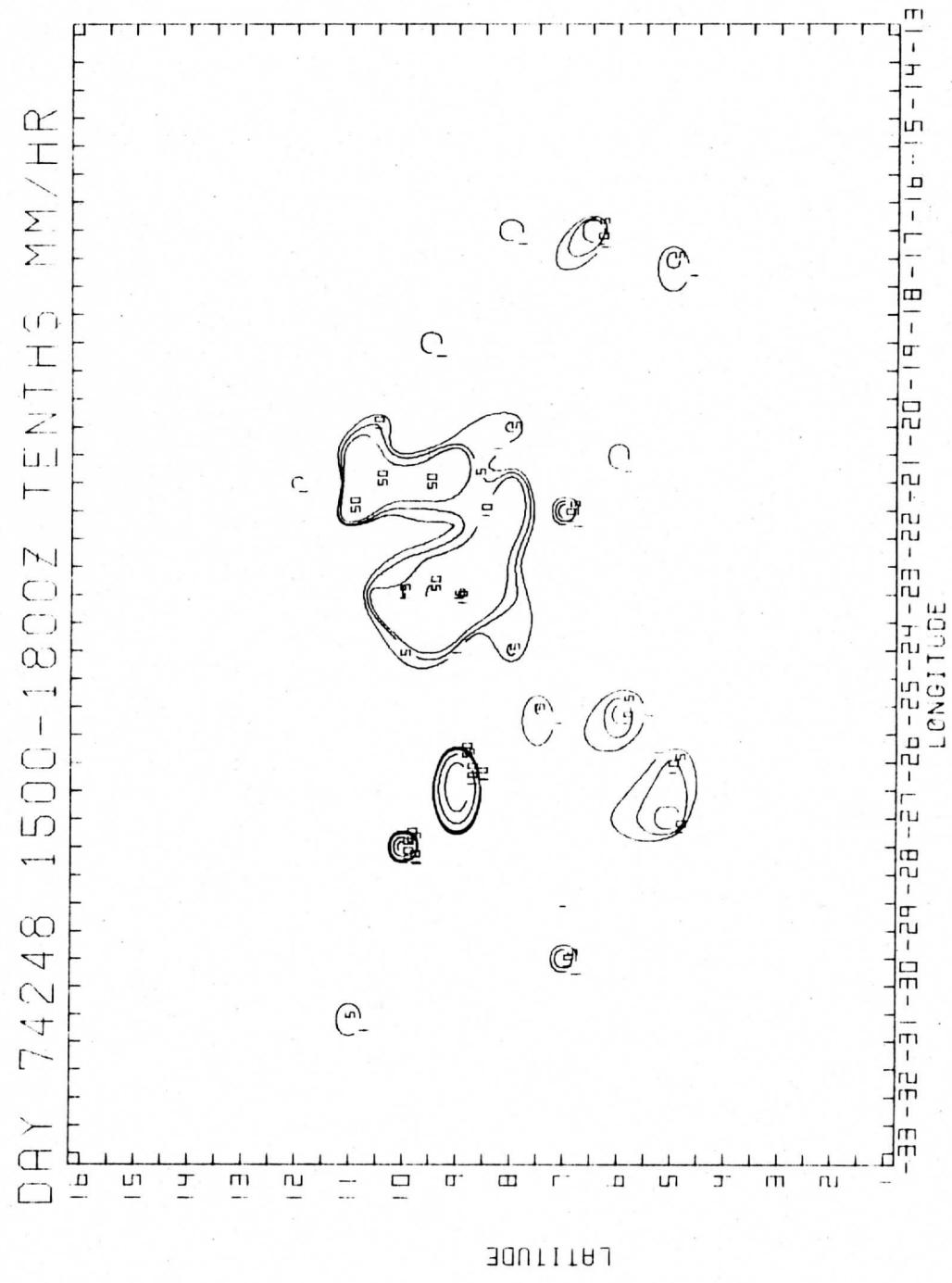
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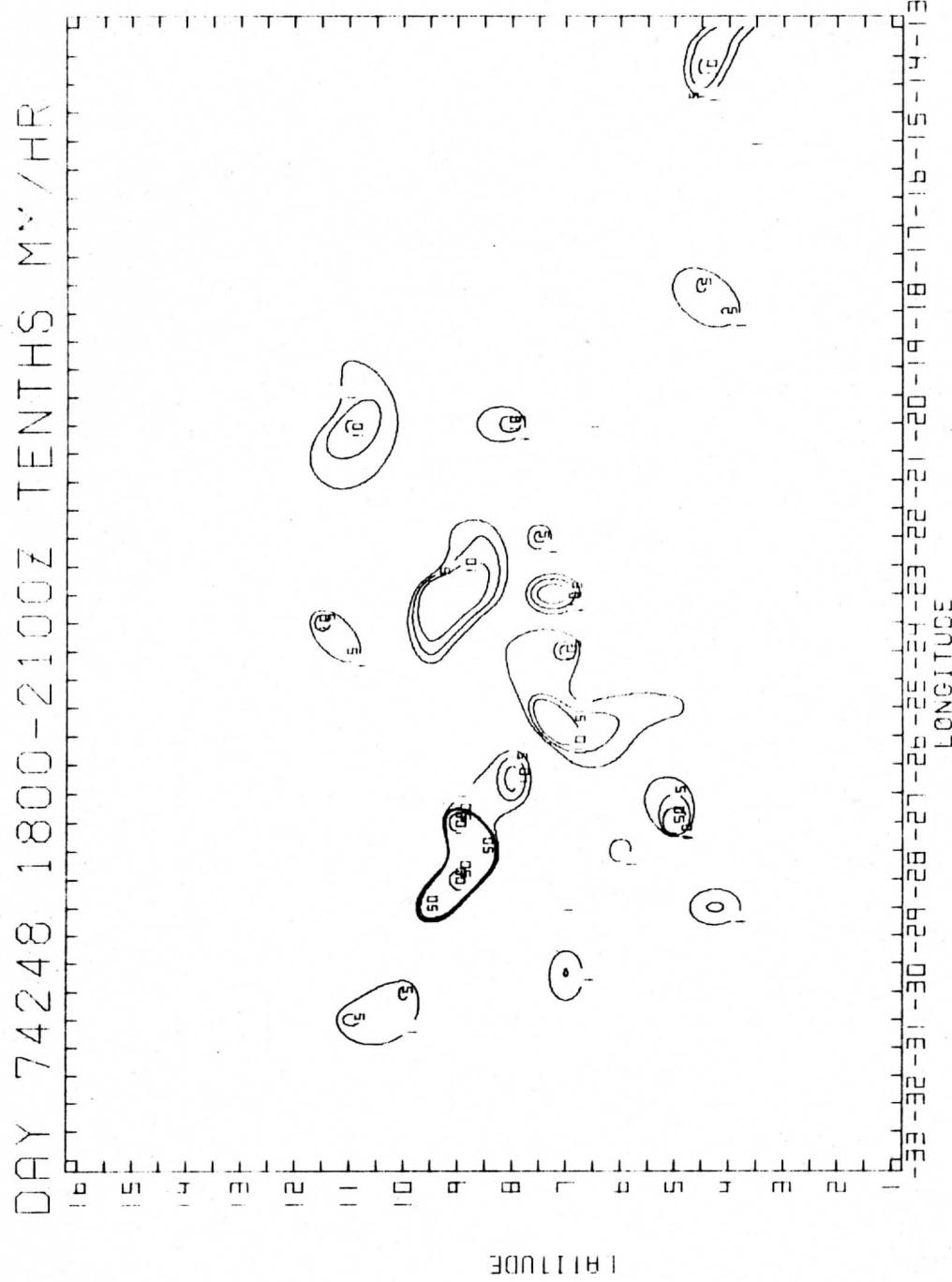
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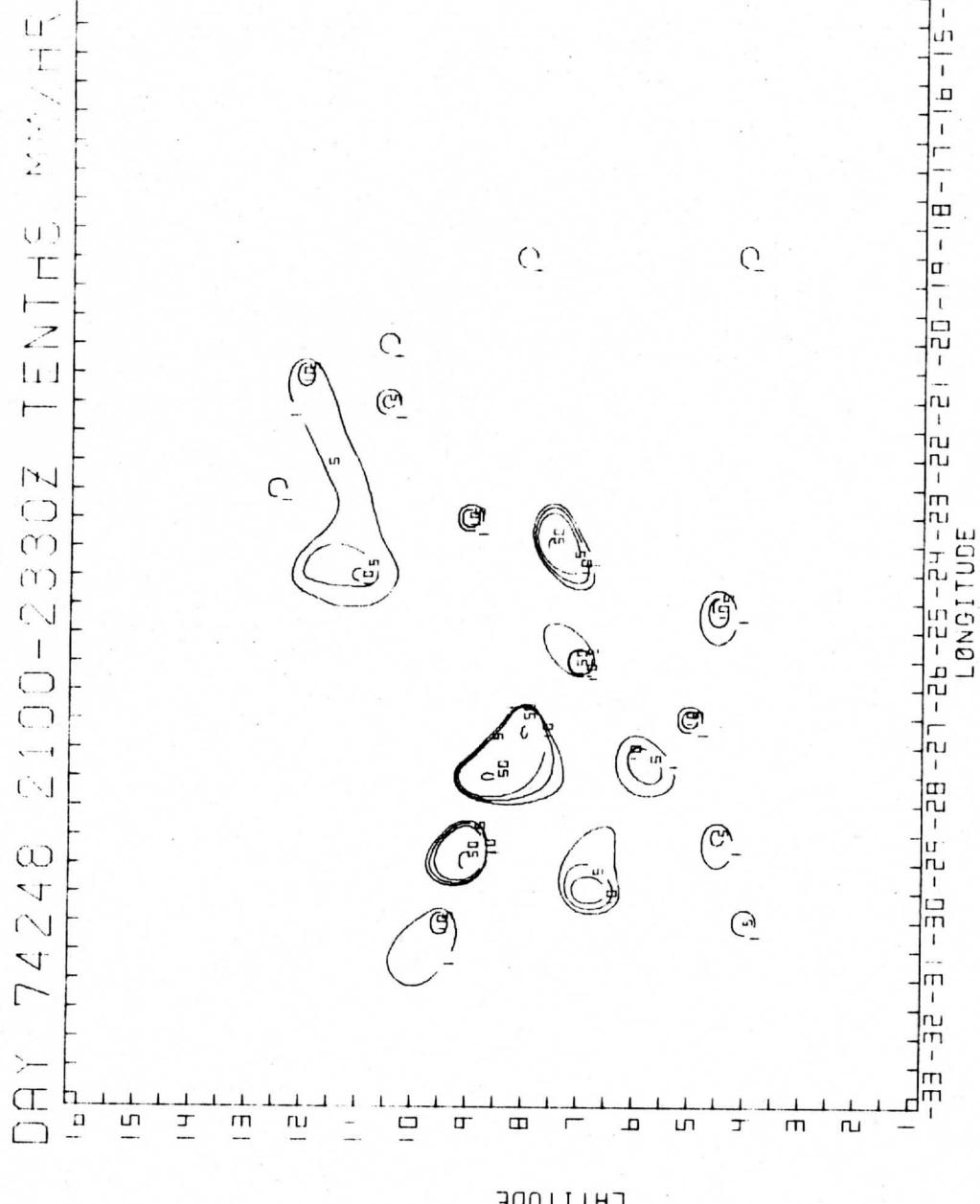
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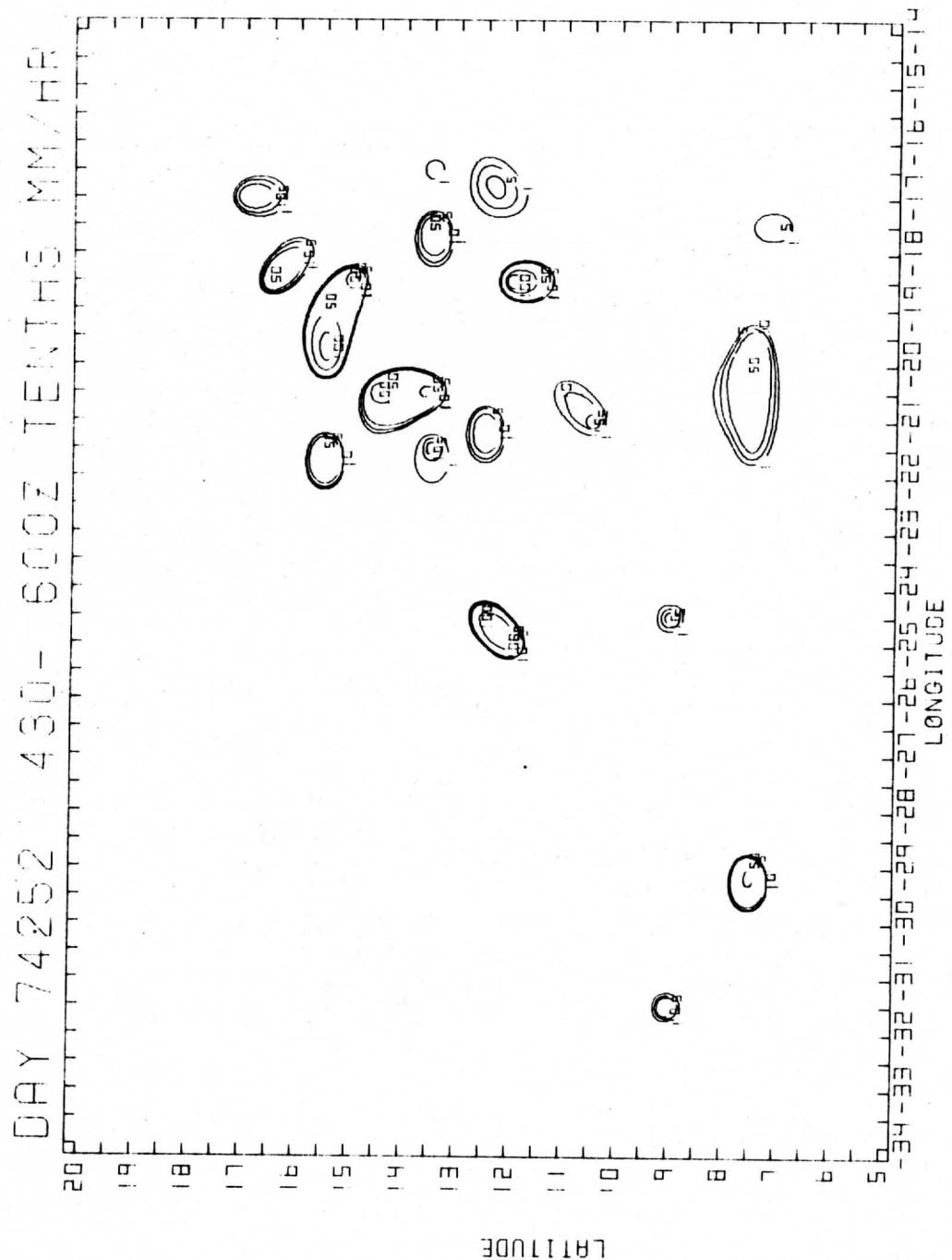
ELEVATION

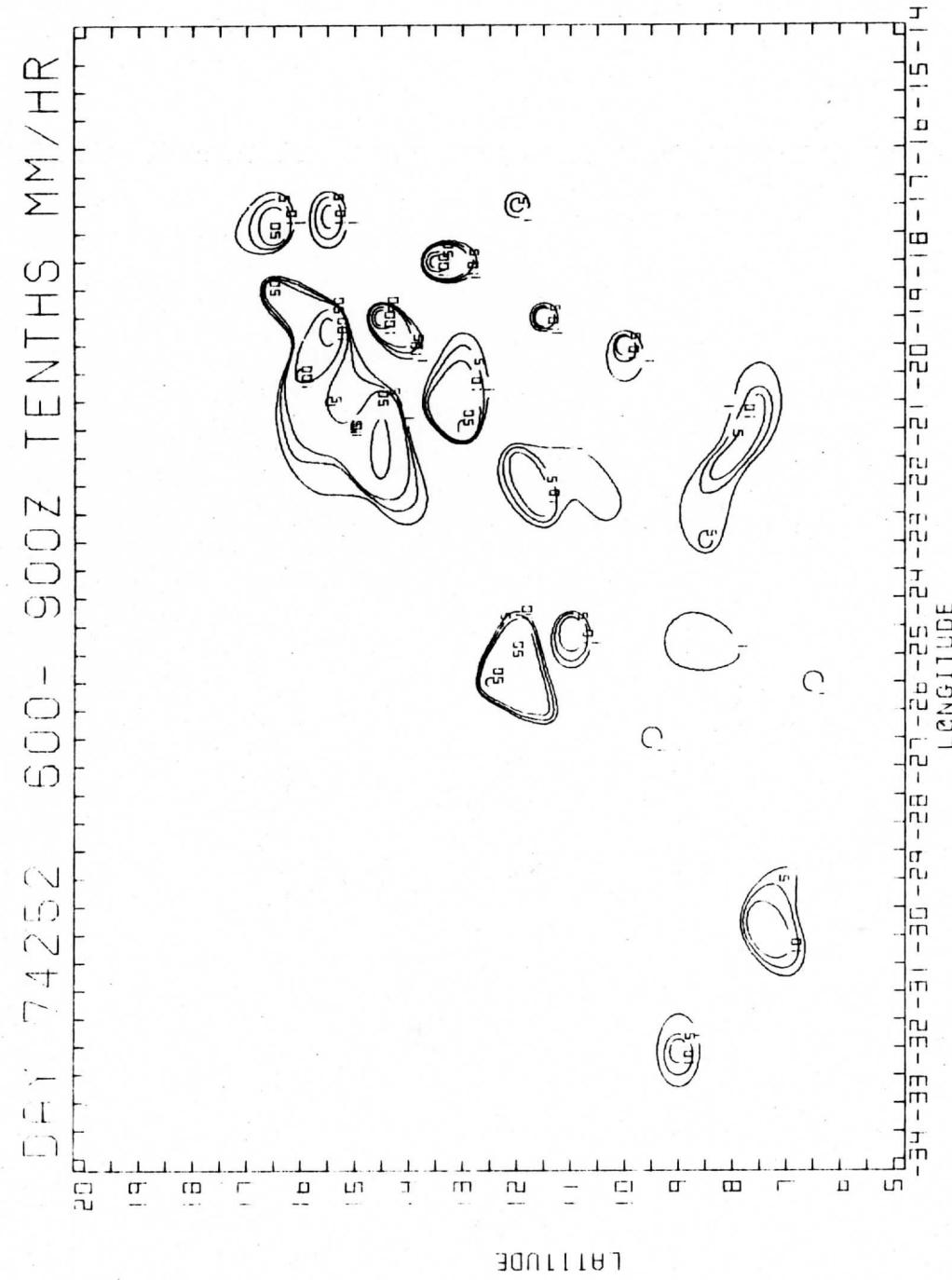


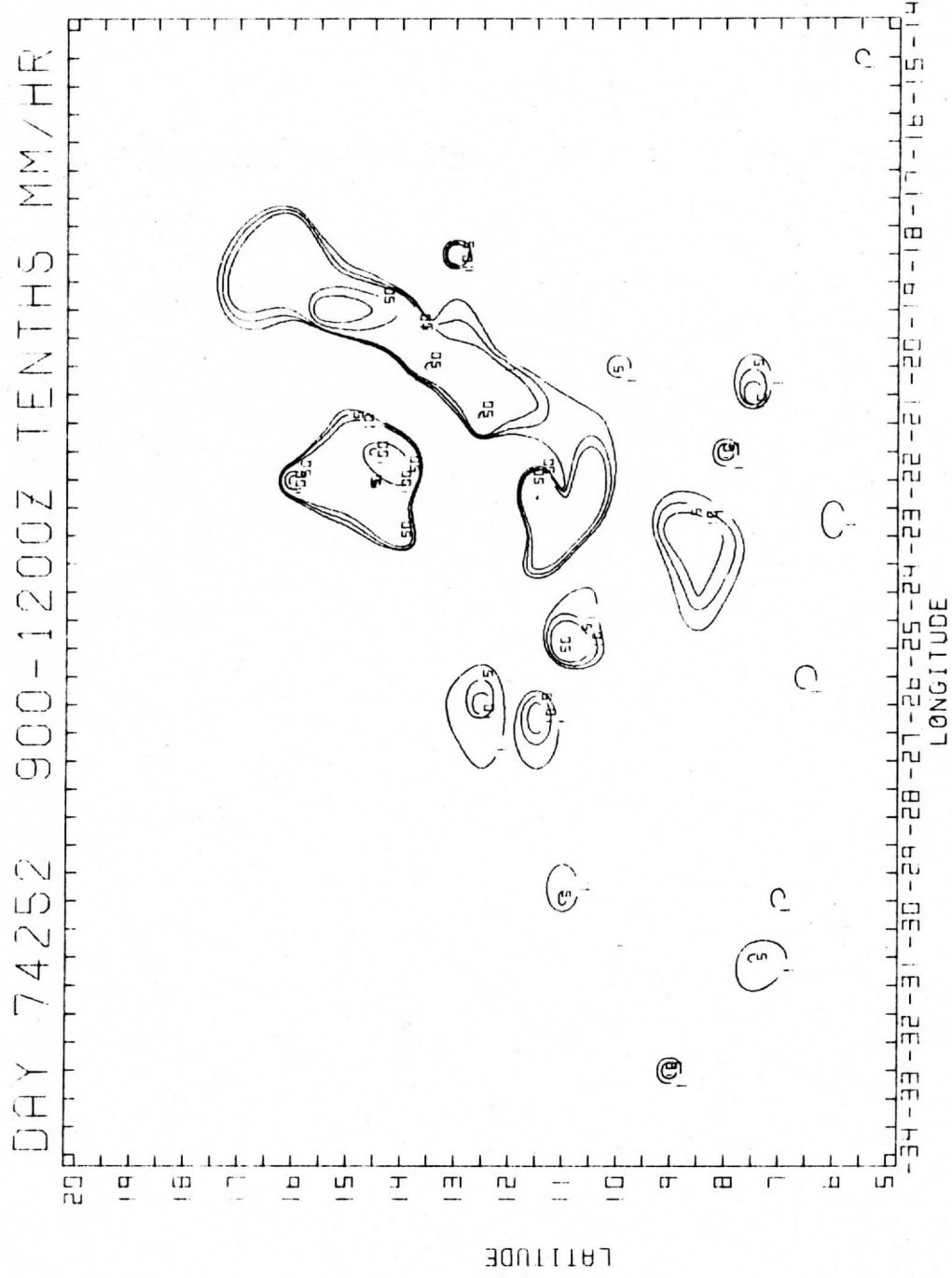


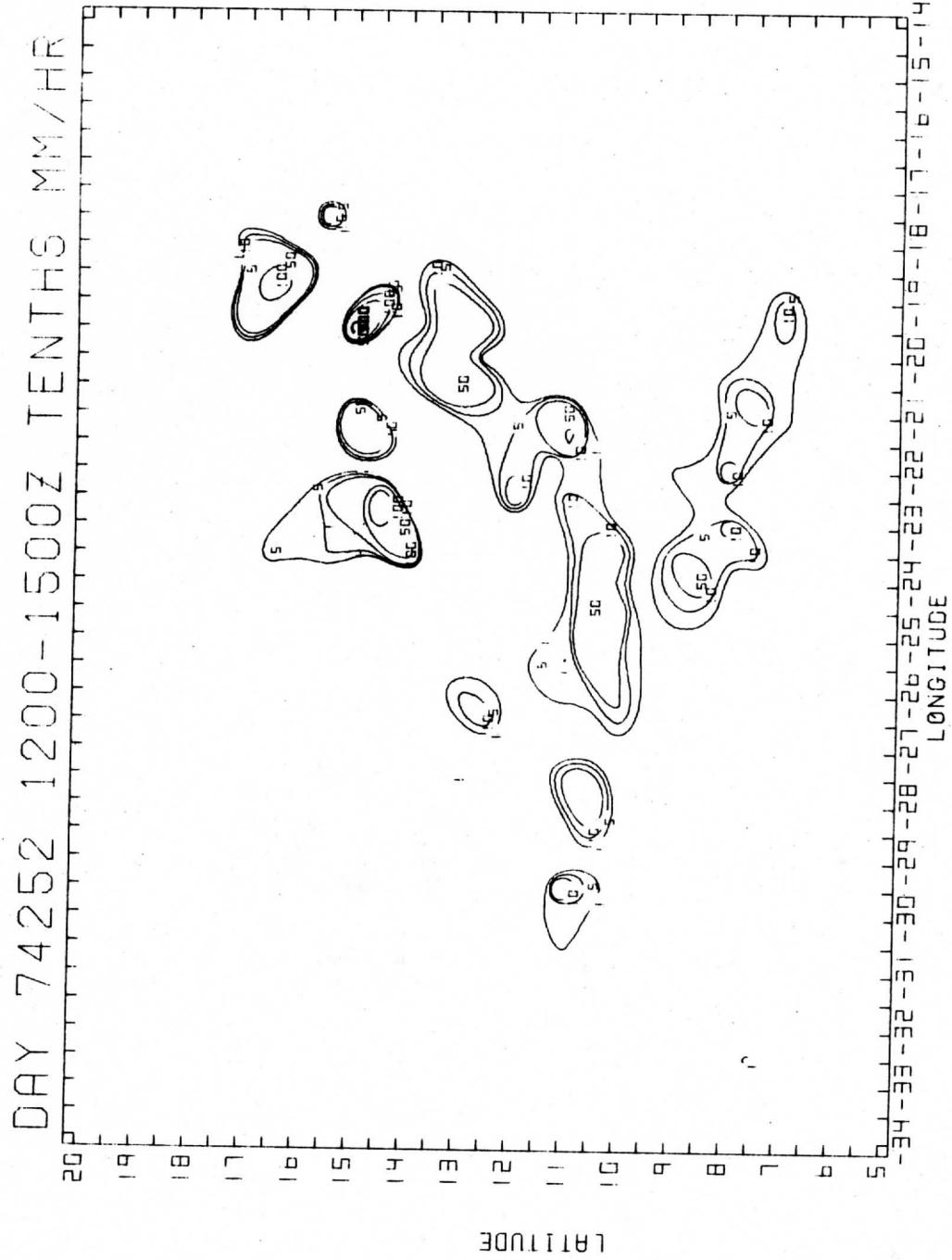


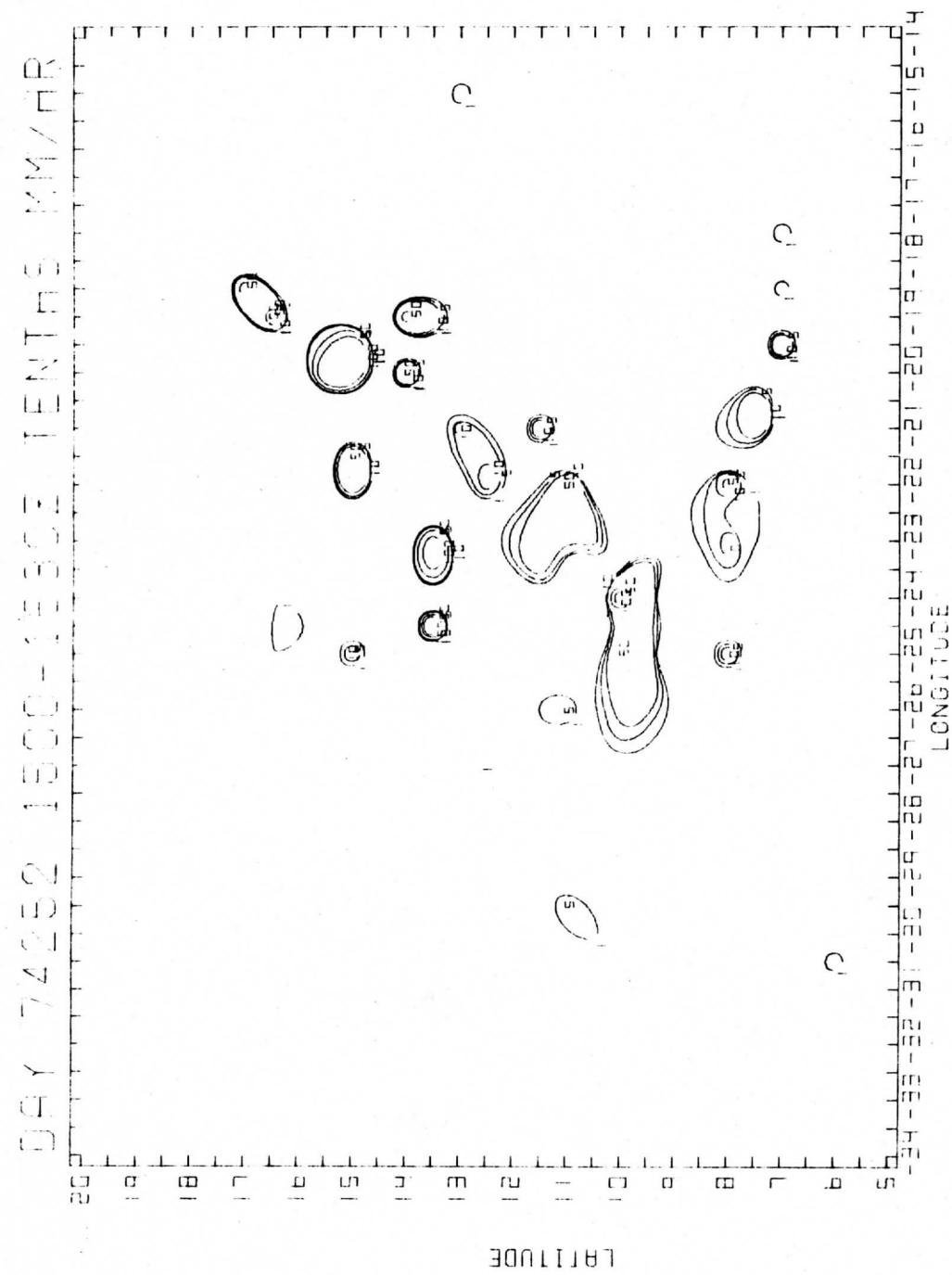


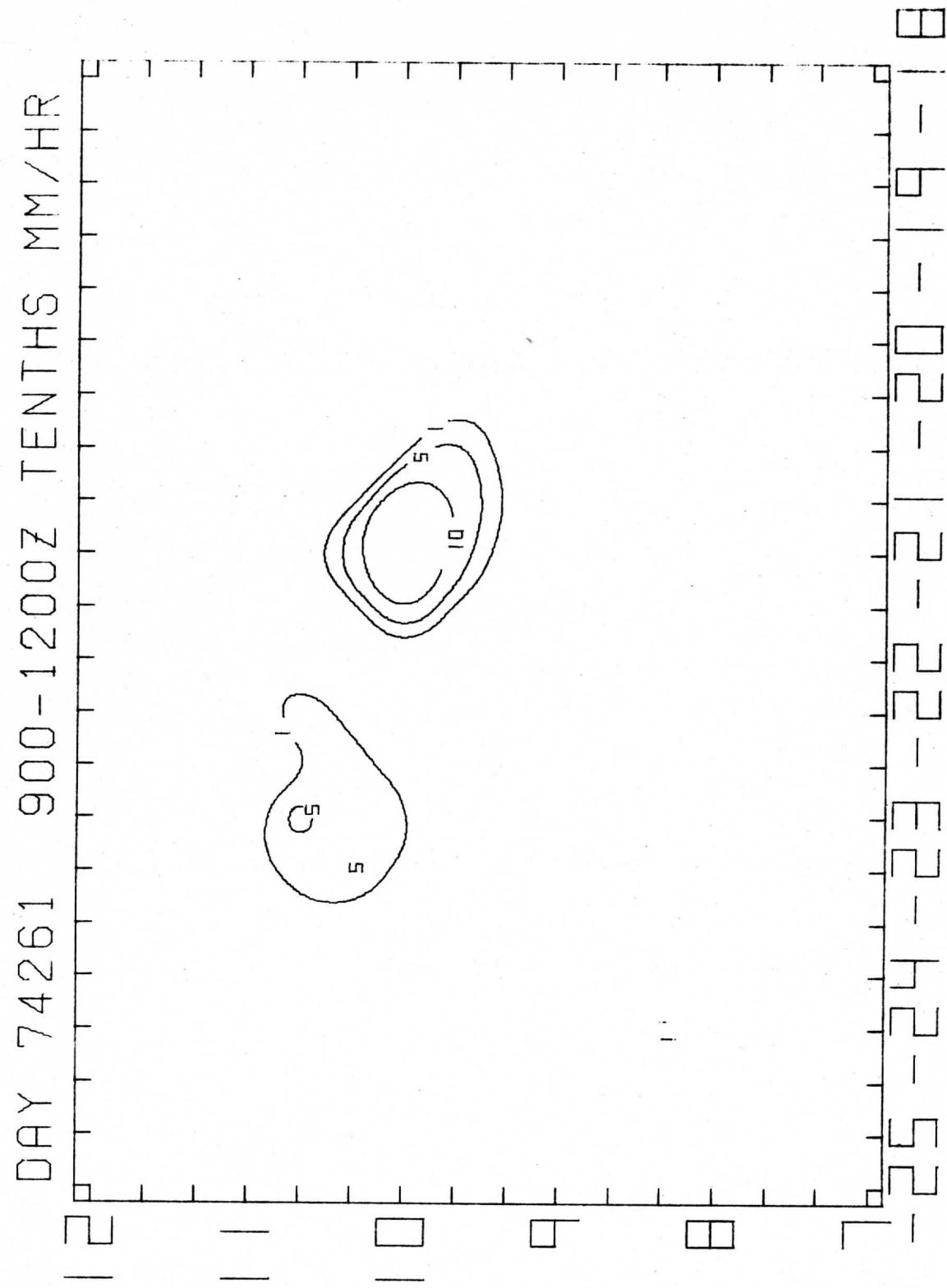




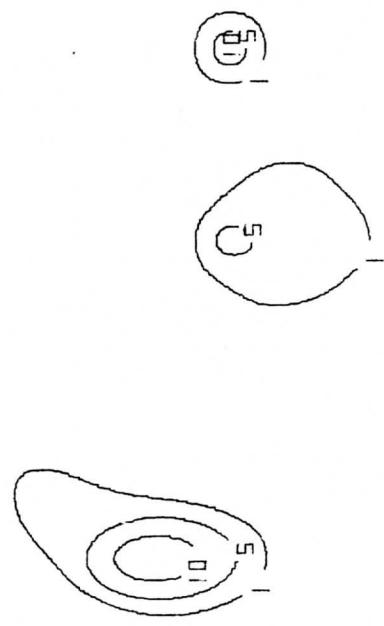








DAY 74261 800 - 900Z TENTHS MM / HR



DAY 74261 1200-1500Z TENTHS MM/HR

